

APPENDIX E

OPEN PIT AND UNDERGROUND MINING

Appendix E1

Open Pit – Design Basis Memorandum

Seabridge Gold Inc.



MINE DESIGN BASIS - KSM PFS UPDATE 2012

2012/06/12

Foreign Exchange Rate \$US : \$C		0.95	\$US/\$C	Wardrop (Tysen) email - 13 Dec 2011	
		\$C	Units	Source	
CONSUMABLE - STANDARD PRICES					
Fuel cost		0.897	\$C/litre	Neil Brazier Email 10 Feb 2012	
Electricity (Energy Charge)		0.0577	\$C/kWhr	Neil Brazier Email 8 Feb 2012	
METAL PRICES					
Copper	\$3.21	\$US/lb.	3.38	\$C/lb.	Wardrop (Tysen) email - 13 Dec 2011
Gold	\$1 244.00	\$US/oz	1309.47	\$C/oz	Wardrop (Tysen) email - 13 Dec 2011
Silver	\$22.98	\$US/oz	24.19	\$C/oz	Wardrop (Tysen) email - 13 Dec 2011
Molybdenum	\$14.14	\$US/lb.	14.88	\$C/lb.	Wardrop (Tysen) email - 13 Dec 2011
TOPOGRAPHY					
NAD 83 - 2009 Lidar		McElhanney 2010			
PRODUCTION TARGETS					
		Mitchell	Sulphurets	Kerr	Iron Cap
AVG Metallurgical Process Daily throughput	tpd	130 000	130 000	130 000	130 000
Metallurgical Process Production days	days	365	365	365	365
Relative production rate	%	115%	88%	123%	112%
Annual Throughput	Mtpa	54.6	41.8	58.4	53.1
Mill annual throughput	tpd	130 000		tpa	47 450 000
Rate Item for MSSP		0.870	1.136	0.813	0.893
Available mine production days	days/yr	355			
Ramp Up:	Year1	Year 2	Year 3		
	58%	94%	100%		

from Schedule 2.2b

Seabridge Gold Inc.

MINE DESIGN BASIS - KSM PFS UPDATE 2012



PROCESS - Mitchell

Recovery and Grade Relationships

Copper			
	Copper Head	Copper Recovery	
	> 1.0% Cu	95%	2011 PFS update
	0.8 - 1.0% Cu	92%	2011 PFS update
	0.227 - 0.8% Cu	= 90.68 x (Cu Head, %)^0.027	2011 PFS update
	0.05 - 0.227% Cu	= 18.02 x ln(Cu Head, %) + 113.5	2011 PFS update
	0.02 - 0.05% Cu	20%	2011 PFS update
	< 0.02%	3%	2011 PFS update
Gold			
	Gold Head	Gold Recovery	
to Copper Concentrate	n/a	= 0.054 x (Cu Recovery, %) ^1.575	2011 PFS update
+			2011 PFS update
To Dore	< 0.1 g/t	0	2011 PFS update
	0.1 - 5 g/t	= (87.491 x (Au Head, g/t)^0.051 - (0.054 x (Cu Recovery, %) ^1.575)) x 68% x 99%	2011 PFS update
	5 - 10 g/t Au	= (95 - (0.054 x (Cu Recovery, %) ^1.575)) x 75% x 99%	2011 PFS update
	> 10 g/t Au	= (98 - (0.054 x (Cu Recovery, %) ^1.575)) x 80% x 99%	2011 PFS update
Total Gold Recovery = Recovery to Copper Concentrate + Recovery to Dore			
Moly			
	Moly Head	Moly Recovery	
	> 0.010%	47%	2011 PFS update
	0.005-0.010% Mo	35%	2011 PFS update
	0.0025-0.005% Mo	25%	2011 PFS update
	<0.0025% Mo	0%	2011 PFS update
		25	2011 PFS update
Silver			
	Silver Head	Silver Recovery	
to Copper Concentrate	n/a	= 1.496 x (Cu Recovery, %) - 76.58	2011 PFS update
To Dore	< 1 g/t Ag	0%	2011 PFS update
	1 - 8 g/t Ag	= (43.16 x (Ag Head, g/t)^0.329) - (1.496 x (Cu Recovery, %) - 76.58); if <0, use 0%	2011 PFS update
	8 - 15 g/t Ag	= 86 - (1.496 x (Cu Recovery, %) - 76.58)	2011 PFS update
	> 15 g/t Ag	= 88 - (1.496 x (Cu Recovery, %) - 76.58)	2011 PFS update
Total Silver Recovery = Recovery to Copper Concentrate + Recovery to Dore			

Process Costs (\$/tonne ORE)

Mitchell	\$/tonne ore	\$/ tonne
Process	6.88	7.24
G&A	1.09	1.15
Surface Service	0.29	0.31
Tailing Construction	0.44	0.46
Total	8.70	9.16
Water Treatment Costs		0.41
TOTAL		9.57
		\$/CDN/tonne ORE

Email From J Huang - Wardrop - 10 February 2012
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PRODUCTION TARGETS

AVG Metallurgical Process Daily throughput	130 000	tpd	
Metallurgical Process Production days	365	days	estimate
Relative production rate	115%		
Annual Throughput	54 567 500	tpa	estimate
Available mine production days	355	days/yr	estimate

Seabridge Gold Inc.

MINE DESIGN BASIS - KSM PFS UPDATE 2012



PROCESS - Sulphurets

Recovery and Grade Relationships

Copper	Copper Head	Copper Recovery	
	> 1.0% Cu	93%	2011 PFS update
	0.8 - 1.0% Cu	90%	2011 PFS update
	0.227 - 0.8% Cu	= $90.68 \times (\text{Cu Head, \%})^{0.027} - 3.5$	2011 PFS update
	0.05 - 0.227% Cu	= $18.02 \times \ln(\text{Cu Head, \%}) + 110$	2011 PFS update
	0.02 - 0.05% Cu	20%	2011 PFS update
	< 0.02%	3%	2011 PFS update
Gold	Gold Head	Gold Recovery	
to Copper Concentrate	n/a	= $0.054 \times (\text{Cu Recovery, \%})^{1.575} - 2$	2011 PFS update
+			2011 PFS update
To Dore	< 0.1 g/t	0	2011 PFS update
	0.1 - 5 g/t	= $(87.491 \times (\text{Au Head, g/t})^{0.051} + 3) - (0.054 \times (\text{Cu Recovery, \%})^{1.575} - 2) \times 49\% \times 99\%$	2011 PFS update
	5 - 10 g/t Au	= $(95 - (0.054 \times (\text{Cu Recovery, \%})^{1.575})) \times 60\% \times 99\%$	2011 PFS update
	> 10 g/t Au	= $(98 - (0.054 \times (\text{Cu Recovery, \%})^{1.575})) \times 70\% \times 99\%$	2011 PFS update
Total Gold Recovery = Recovery to Copper Concentrate + Recovery to Dore			
Moly	Moly Head	Moly Recovery	
	> 0.010%	47%	2011 PFS update
	0.005-0.010% Mo	35%	2011 PFS update
	0.0025-0.005% Mo	25%	2011 PFS update
	<0.0025% Mo	0%	2011 PFS update
Silver	Silver Head	Silver Recovery	
to Copper Concentrate	n/a	35%	2011 PFS update
To Dore	< 1 g/t Ag	0%	2011 PFS update
	1 - 8 g/t Ag	= $(43.16 \times (\text{Ag Head, g/t})^{0.329}) - 35.3$	2011 PFS update
	8 - 15 g/t Ag	50.7%	2011 PFS update
	> 15 g/t Ag	52.7%	2011 PFS update
Total Silver Recovery = Recovery to Copper Concentrate + Recovery to Dore			

Process Costs (\$/tonne ORE)

Sulphurets	\$/US/tonne ore	\$/CDN/tonne
Process	7.45	7.84
G&A	1.09	1.15
Surface Service	0.29	0.31
Tailing Construction	0.44	0.46
Total	9.27	9.76
Water Treatment Costs		0.41
TOTAL		10.17
		\$/CDN/tonne ORE

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PRODUCTION TARGETS

AVG Metallurgical Process Daily throughput	130 000	tpd	
Metallurgical Process Production days	365	days	estimate
Relative production rate	88%		
Annual Throughput	41 756 000	tpa	estimate
Available mine production days	355	days/yr	estimate

Seabridge Gold Inc.

MINE DESIGN BASIS - KSM PFS UPDATE 2012



PROCESS - Mitchell

Recovery and Grade Relationships

Copper	Copper Head	Copper Recovery	
	> 1.0% Cu	84%	2011 PFS update
	0.8 - 1.0% Cu	81%	2011 PFS update
	0.227 - 0.8% Cu	= $90.68 \times (\text{Cu Head, \%})^{\wedge} 0.027 - 9$	2011 PFS update
	0.05 - 0.227% Cu	= $18.02 \times \ln(\text{Cu Head, \%}) + 104.5$	2011 PFS update
	0.02 - 0.05% Cu	20%	2011 PFS update
	< 0.02%	3%	2011 PFS update
Gold	Gold Head	Gold Recovery	
to Copper Concentrate	n/a	= $0.054 \times (\text{Cu Recovery, \%})^{\wedge} 1.575 - 18$	2011 PFS update
+			2011 PFS update
To Dore	< 0.1 g/t	0%	2011 PFS update
	0.1 - 5 g/t	= $(87.491 \times (\text{Au Head, g/t})^{\wedge} 0.051 + 8) - (0.054 \times (\text{Cu Recovery, \%})^{\wedge} 1.575 - 18)) \times 68\% \times 99\%$	2011 PFS update
	5 - 10 g/t Au	= $(95 - (0.054 \times (\text{Cu Recovery, \%})^{\wedge} 1.575 - 18)) \times 75\% \times 99\%$	2011 PFS update
	> 10 g/t Au	= $(98 - (0.054 \times (\text{Cu Recovery, \%})^{\wedge} 1.575 - 18)) \times 80\% \times 99\%$	2011 PFS update
Total Gold Recovery = Recovery to Copper Concentrate + Recovery to Dore			
Moly	Moly Head	Moly Recovery	
	> 0.010%	47%	2011 PFS update
	0.005-0.010% Mo	35%	2011 PFS update
	0.0025-0.005% Mo	25%	2011 PFS update
	<0.0025% Mo	0%	2011 PFS update
Silver	Silver Head	Silver Recovery	
to Copper Concentrate	n/a	37%	2011 PFS update
To Dore	< 1 g/t Ag	0%	2011 PFS update
	1 - 8 g/t Ag	= $(21.26 \times \ln(\text{Ag Head, g/t}) + 40.74) - 37$	2011 PFS update
	8 - 15 g/t Ag	49%	2011 PFS update
	> 15 g/t Ag	51%	2011 PFS update
Total Silver Recovery = Recovery to Copper Concentrate + Recovery to Dore			

Process Costs (\$/tonne ORE)

Kerr	\$/tonne ore	\$/ tonne
Process	6.92	7.28
G&A	1.09	1.15
Surface Service	0.29	0.31
Tailing Construction	0.44	0.46
Total	8.74	9.20
Water Treatment Costs		0.41
TOTAL		9.61
		\$/CDN/tonne ORE

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PRODUCTION TARGETS

AVG Metallurgical Process Daily throughput	130 000	tpd	
Metallurgical Process Production days	365	days	estimate
Relative production rate	123%		
Annual Throughput	58 363 500	tpa	estimate
Available mine production days	355	days/yr	estimate

Seabridge Gold Inc.

MINE DESIGN BASIS - KSM PFS UPDATE 2012



PROCESS - Mitchell

Recovery and Grade Relationships

Copper	Copper Head	Copper Recovery	
	> 1.0% Cu	95%	2011 PFS update
	0.8 - 1.0% Cu	92%	2011 PFS update
	0.227 - 0.8% Cu	= 90.68 x (Cu Head, %)^0.027	2011 PFS update
	0.05 - 0.227% Cu	= 18.02 x ln(Cu Head, %) + 113.5	2011 PFS update
	0.02 - 0.05% Cu	20%	2011 PFS update
	< 0.02%	3%	2011 PFS update
Gold	Gold Head	Gold Recovery	
to Copper Concentrate	< 8 g/t Au	= 7.457 x ln(Au Head, g/t) + 53.88	2011 PFS update
+	> 8 g/t Au	70%	2011 PFS update
To Dore	< 0.1 g/t	0	2011 PFS update
	0.1 - 8 g/t	= (4.278 x ln(Au Head, g/t) + 69.62) - (7.457 x ln(Au Head, g/t) + 53.88)	2011 PFS update
	8 - 20 g/t Au	= (4.278 x ln(Au Head, g/t) + 69.62) - 70	2011 PFS update
	> 20 g/t Au	20%	2011 PFS update
Total Gold Recovery = Recovery to Copper Concentrate + Recovery to Dore			
Moly	Moly Head	Moly Recovery	
	> 0.010%	47%	2011 PFS update
	0.005-0.010% Mo	35%	2011 PFS update
	0.0025-0.005% Mo	25%	2011 PFS update
	<0.0025% Mo	0%	2011 PFS update
Silver	Silver Head	Silver Recovery	
to Copper Concentrate	n/a	61%	2011 PFS update
To Dore	< 1 g/t Ag	0%	2011 PFS update
	1 - 8 g/t Ag	= (21.26 x ln(Ag Head, g/t) + 40.74) - 61	2011 PFS update
	8 - 15 g/t Ag	25%	2011 PFS update
	> 15 g/t Ag	27%	2011 PFS update
Total Silver Recovery = Recovery to Copper Concentrate + Recovery to Dore			

Process Costs (\$/tonne ORE)

Iron Cap	\$/US/tonne ore	\$/C / tonne
Process	6.88	7.24
G&A	1.09	1.15
Surface Service	0.29	0.31
Tailing Construction	0.44	0.46
Total	8.70	9.16
Water Treatment Costs		0.41
TOTAL		9.57
		\$/CDN/tonne ORE

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PRODUCTION TARGETS

AVG Metallurgical Process Daily throughput	130 000	tpd	
Metallurgical Process Production days	365	days	estimate
Relative production rate	112%		
Annual Throughput	53 144 000	tpa	estimate
Available mine production days	355	days/yr	estimate

Seabridge Gold Inc.



Pit Optimization - Net Smelter Revenues and Prices

Description	Variable	Calculation	Values	Previous	Units
Average Mill Feed Grades					
Gold	Au	Input	0.546	0.586	g/t
Copper	Cu	Input	0.207	0.199	%
Silver	Ag	Input	3.04	2.58	g/t
Molybdenum	Mo	Input	53.2	59.4	ppm
Process Recovery to Copper Concentrate					
Gold	CCAuRec	= 0.054 x (Cu Recovery, %) ^1.575	61.1	58.5	%
Copper	CCCuRec	= 90.68 x (Cu Head, %) ^0.027	86.9	83.5	%
Silver	CCAgRec	= 1.496 x (Cu Recovery, %) - 76.58	53.4	55.0	%
Process Recovery to Gold Dore					
Gold	GDAuRec	= (87.491 x (Au Head, g/t) ^0.051 - (0.054 x (Cu Recovery, %) ^1.575)) x 68%	15.9	19.0	%
Silver	GDAgRec	= (43.16 x (Ag Head, g/t) ^0.329) - (1.496 x (Cu Recovery, %) - 76.58)	8.8	18.0	%
Concentrate Specs					
Copper grade	ConCu	constant (Head Grade 0.15 - 0.4% Cu)	24.0		%
Gold Grade	ConAu	=(CCAuRec / 100 x Au) / (Cu x (CCCuRec/100) / ConCu)	44.5		gpt
Silver Grade	ConAg	=(CCAgRec / 100 x Ag) / (Cu x (CCCuRec/100) / ConCu)	217		gpt
Molybdenum	ConMo	constant	50%		%
Moisture Cu Con	cmoCu	Input	9%		%
Moisture Mo Con	cmoMo	Input	5%		%
Prices					
Gold Price	AUPRC	Input	\$1 244	\$990	US\$/oz
Copper Price	CUPRC	Input	\$3.21	\$2.91	US\$/lb
Silver Price	AGPRC	Input	\$22.98	\$15.40	US\$/oz
Molybdenum Price	MoPRC	Input	\$14.14	\$15.00	US\$/lb
US Exchange rate	XRATE	Input	0.950	0.93	US\$/CDNS
Gold Price	AUCDN	=AUPRC/XRATE/gpoz	42.10		CDNS/g
Copper Price	CUCDN	=CUPRC/XRATE	3.379		CDNS/lb
Silver Price	AGCDN	=AGPRC/XRATE/gpoz	0.778		CDNS/q
Molybdenum Price	MoCDN	=MoPRC/XRATE	14.88		CDNS/lb
Conversions					
Pounds per tonne conversion	ppt	Constant	2204.62		lb/tonne
Grams per ounce conversion	gpoz	Constant	31.10348		g/oz
MoS2 to Mo		Constant	0.599		Mo/MoS2
Smelter Terms					
Copper Conc.					
cu unit deductions	dedcu	Input	1.0%		%
au payable	pavau	Input	97.5%		%
ag payable	payag	Input	90%		%
smelting	smelt	Input	85.000		US\$/DMT
cu refining - base	refcuca	Input	0.085		US\$/lb
price participation (cu floor)	prpart	Input	1.500		US\$/lb
price participation % for amount above prpart	prpart%	Input	1.5%		%
Price Participation Cap	prpartCAP	Input	0.040		US\$/lb
Price Participation	PP	MIN((CUPRC-prpart) "prpart%	0.026		US\$/lb
cu refining - with participation	refcu	refcuca + PP	0.111		US\$/lb
au refining	refau	Input	3.000		US\$/oz
ag refining	refag	Input	0.600		US\$/oz
Moly Conc.					
Mo payable	paymo	Input	99.0%		%
Losses in handling and roasting	dedMo	Input	4.20%		%
Roasting	smelt	Input	2.00		US\$/lb
Mo refining - base	refmoa	Input	0.000		US\$/lb
Dry Concentrate tonnes					
Copper Conc	DMTCu	= 1-cmoCu	91%		%
Moly Conc	DMTMo	= 1-cmoMo	95%		%

Net Copper Revenue per Tonne Copper Conc.					
Cu in Conc	NetCu	= DMTCu*ConCu*ppt	481.49		lb/WMT
Net payable Cu in Concentrate	NPYCu	= DMTCu*(ConCu-dedcu)*ppt	461.43		lb/WMT
Net payment Cu in Concentrate	PayCu	= NPYCu/CLUCDN	\$1 559.14		CDNS/WMT
Refining Cu	CuRef	= NetCu*refcu/XRATE	\$56.08		CDNS/WMT
Net Revenue Copper	NRcu	= PayCu-CuRef	\$1 503.06		CDNS/WMT
Net Gold Revenue per Tonne Copper Conc.					
Au in Conc	NetAu	= DMTCu*ConAu	40.53		g/WMT
Net payable Au in Concentrate	NPYAu	= payau*NetAu	39.52		g/WMT
Net payment Au in Concentrate	PayAu	= NPYAu/AUCDN	\$1 663.84		CDNS/WMT
Refining Au	AuRef	= NetAu*refau/XRATE/gpoz	\$10.70		CDNS/WMT
Net Revenue Gold	NRAu	= PayAu-AuRef	\$1 653.14		CDNS/WMT
Net Silver Revenue per Tonne Copper Conc.					
Ag in Conc	NetAg	= DMT*ConAg	197.19		g/WMT
Net payable Ag in Concentrate	NPYAg	= payag*NetAg	177.47		g/WMT
Net payment Ag in Concentrate	PayAg	= NPYAg*AgCDN	\$138.02		CDNS/WMT
Refining Ag	AgRef	= NetAg*refag/XRATE/gpoz	\$3.60		CDNS/WMT
Net Revenue Silver	NRAg	= PayAg-AgRef	\$134.42		CDNS/WMT
Net Revenue Total Copper Conc					
Proportion Copper	TRCu	= NRCu + NRAu + NRAg	\$3 290.61		CDNS/WMT
Proportion Gold	TRAu	= NRAu/TRev	45.68%		%
Proportion Silver	TRAg	= NRAg/TRev	50.24%		%
			4.08%		%
Offsites, Freight, and Distribution Copper Conc					
Smelting	Smelt	=smelt*DMT/XRATE	\$81.42		CDNS/WMT
freight for trucking	truck	Input	\$32.94		CDNS/WMT
freight for rail	frail	Input			CDNS/WMT
Stevedoring	fsteve	Input			USS/WMT
freight for ships	focean	Input	\$67.99		USS/WMT
Other Offsite Costs (Losses, Ins, Sell, supv, Assay)	other	Input	\$16.47		CDNS/WMT
Offsites, Frgt, Distr, Total	OFD	= Sum (Smelt : Other)	\$202.40		CDNS/WMT
Proportion Copper	OFDCu	=OFD*TRCu	\$92.45		CDNS/WMT
Proportion Gold	OFDAu	=OFD*TRAu	\$101.68		CDNS/WMT
Proportion Silver	OFDAg	=OFD*TRAg	\$8.27		CDNS/WMT
Net Moly Revenue per Tonne Moly Conc.					
Mo in Conc	NetMo	= DMT*ConMo*ppt	1047.19		lb/WMT
Net payable Mo in Concentrate	NPYMo	= (paymo-dedMo)*NetMo	992.74		lb/WMT
Net payment Mo in Concentrate	paymo	= NPYMo/MoCDN	\$14 776.16		CDNS/WMT
Refining Mo	MoRef	= NetMo*refmo	\$0.00		CDNS/WMT
Net Revenue Moly	NRMo	= paymo-MoRef	\$14 776.16		CDNS/WMT
Offsites, Freight, and Distribution Moly Conc					
Roasting & Smelting	smelt	smelt*ppt/DMT/XRATE	\$4 409.24		CDNS/WMT
Trucking	truck	Input	\$66.96		CDNS/WMT
Rail	frail	Input			CDNS/WMT
Ocean Freight	focean	Input	\$88.93		USS/WMT
Other Offsite Costs (Losses, Ins, Sell, supv, Assay)	other	Input	\$50.00		CDNS/WMT
Offsites, Frgt, Distr, Total	OFD	= Sum (Smelt : Other)	\$4 619.81		CDNS/WMT
Proportion Molybdenum	OFDMo	=OFD	\$4 619.81		CDNS/WMT
Gold Dore					
Au Payable	auDpav	Input	99.6		%
au refining + transport	auDref	Input	2.00		USS/oz
	auDTr	Input			CDNS/Tonne
Au Dore NSP	auDNsp	=AUCDN*AuDpay/100-AuDref/XRATE/gpoz-auDTr/1000	41.88		CDNS/q
Ag Dore NSP	agDNsp		0.707		CDNS/g
Au distribution to Dore	AuDR	Au in Dore / (Au in Dore + Au in Cu Conc.)	21%		%
Ag distribution to Dore	AgDR	Ag in Dore / (Ag in Dore + Ag in Cu Conc.)	14%		%
Net Smelter Return per Tonne Cu Conc. (Wet)					
NSR Copper	NSRCu	= NRCu - OFDCu	\$1 410.61		CDNS/WMT
NSR Gold	NSRAu	= NRAu - OFDAu	\$1 551.45		CDNS/WMT
NSR Silver	NSRAg	= NRAg - OFDAg	\$126.15		CDNS/WMT
NSR Total	NSR	= NSRCu + NSRAu + NSRAg + NSGMO	\$3 088.21		CDNS/WMT
Net Smelter Return per Tonne Mo Conc. (Wet)					
NSR Moly	NSRMo	= NRMo - OFDMo	\$10 156.35		CDNS/WMT
Net Smelter Price (to Mine Gate)					
Copper	NSPCu	= NSRCu/NetCu	\$2.93		CDNS/lb
Gold	NSPAu	= NSRAu/NetAu x AuCR/(AuDR + AuCR) + auDNsp x AuDR/(AuDR + AuCR)	\$39.02		CDNS/g
Silver	NSPAq	= NSRAg/NetAg	\$0.649		CDNS/q
Moly	NSPMo	= NSRMo/NetMo	\$9.70		CDNS/lb
		NSR = RCU*22.046*2.93+RALP*39.04+RAG*0.649+RMO/1000*22.046*9.70			

Net Copper Revenue per Tonne Copper Conc.			Values	Units
Cu in Conc	NetCu	= DMTCu*ConCu*ppt	481.49	lb/WMT
Net payable Cu in Concentrate	NPYu	= DMTCu*(ConCu-dedcu)*ppt	461.43	lb/WMT
Net payment Cu in Concentrate	PayCu	= NPYu*CUICDN	\$1 559.14	CDNS/WMT
Refining Cu	CuRef	= NetCu*refcu*XRATE	\$56.08	CDNS/WMT
Net Revenue Copper	NRcu	= PayCu-CuRef	\$1 503.06	CDNS/WMT
Net Gold Revenue per Tonne Copper Conc.				
Au in Conc	NetAu	= DMTCu*ConAu	40.53	g/WMT
Net payable Au in Concentrate	NPYu	= payau*NetAu	39.52	g/WMT
Net payment Au in Concentrate	PayAu	= NPYu*AUICDN	\$1 663.84	CDNS/WMT
Refining Au	AuRef	= NetAu*refau*XRATE/gpoz	\$10.70	CDNS/WMT
Net Revenue Gold	NRau	= PayAu-AuRef	\$1 653.14	CDNS/WMT
Net Silver Revenue per Tonne Copper Conc.				
Ag in Conc	NetAg	= DMT*ConAg	197.19	g/WMT
Net payable Ag in Concentrate	NPYu	= payag*NetAg	177.47	g/WMT
Net payment Ag in Concentrate	PayAg	= NPYu*AgICDN	\$138.02	CDNS/WMT
Refining Ag	AgRef	= NetAg*refag*XRATE/gpoz	\$3.60	CDNS/WMT
Net Revenue Silver	NRag	= PayAg-AgRef	\$134.42	CDNS/WMT
Net Revenue Total Copper Conc			\$3 290.61	CDNS/WMT
Proportion Copper	TRCu	= NRCu*TRRev	45.68%	%
Proportion Gold	TRAu	= NRau*TRRev	50.24%	%
Proportion Silver	TRAg	= NRag*TRRev	4.08%	%
Offsites, Freight, and Distribution Copper Conc				
Smelting	Smelt	=smelt*DMT*XRATE	\$81.42	CDNS/WMT
freight for trucking	truck	Input	\$32.94	CDNS/WMT
freight for rail	frail	Input		CDNS/WMT
Stevedoring	fsteve	Input		USS/WMT
freight for ships	focsea	Input	\$67.99	USS/WMT
Other Offsite Costs (Losses, Ins, Sell, supv, Assay)	other	Input	\$16.47	CDNS/WMT
Offsites, Frgt, Distr, Total	OFD	= Sum (Smelt : Other)	\$202.40	CDNS/WMT
Proportion Copper	OFDCu	=OFD*TRCu	\$92.45	CDNS/WMT
Proportion Gold	OFDAu	=OFD*TRAu	\$101.68	CDNS/WMT
Proportion Silver	OFDAg	=OFD*TRAg	\$8.27	CDNS/WMT
Net Moly Revenue per Tonne Moly Conc.				
Mo in Conc	NetMo	= DMT*ConMo*ppt	1047.19	lb/WMT
Net payable Mo in Concentrate	NPYu	= (paymo-dedmo)*NetMo	992.74	lb/WMT
Net payment Mo in Concentrate	paymo	= NPYu*MoICDN	\$14 776.16	CDNS/WMT
Refining Mo	MoRef	= NetMo*refmo	\$0.00	CDNS/WMT
Net Revenue Moly	NRMo	= paymo-MoRef	\$14 776.16	CDNS/WMT
Offsites, Freight, and Distribution Moly Conc				
Roasting & Smelting	smelt	=smelt*ppt/DMT*XRATE	\$4 409.24	CDNS/WMT
Trucking	truck	Input	\$66.96	CDNS/WMT
Rail	frail	Input		CDNS/WMT
Ocean Freight	focsea	Input	\$88.93	USS/WMT
Other Offsite Costs (Losses, Ins, Sell, supv, Assay)	other	Input	\$50.00	CDNS/WMT
Offsites, Frgt, Distr, Total	OFD	= Sum (Smelt : Other)	\$4 619.81	CDNS/WMT
Proportion Molybdenum	OFDMo	=OFD	\$4 619.81	CDNS/WMT
Gold Dore				
Au Payable	auDpav	Input	99.6	%
au refining + transport	auDref	Input	2.00	US\$/oz
Au Dore NSP	auDNsp	Input	41.88	CDNS/Tonne
Ag Dore NSP	agDNsp	=AUCDN*AuDpay/100-AuDref*XRATE/gpoz-auDTr/1000	0.707	CDNS/g
Au distribution to Dore	AuDR	Au in Dore / (Au in Dore + Au in Cu Conc.)	21%	%
Ag distribution to Dore	AgDR	Ag in Dore / (Ag in Dore + Ag in Cu Conc.)	14%	%
Net Smelter Return per Tonne Cu Conc. (Wet)				
NSR Copper	NSRCu	= NRCu - OFDCu	\$1 410.61	CDNS/WMT
NSR Gold	NSRAu	= NRau - OFDAu	\$1 551.45	CDNS/WMT
NSR Silver	NSRag	= NRag - OFDAg	\$126.15	CDNS/WMT
NSR Total	NSR	= NSRCu + NSRAu + NSRag + NSGMo	\$3 088.21	CDNS/WMT
Net Smelter Return per Tonne Mo Conc. (Wet)				
NSR Moly	NSRMo	= NRMo - OFDMo	\$10 156.35	CDNS/WMT
Net Smelter Price (to Mine Gate)				
Copper	NSPCu	= NSRCu/NetCu	\$2.93	CDNS/lb
Gold	NSPAu	= NSRAu/NetAu x AuCR/(AuDR + AuCR) + auDNsp x AuDR/(AuDR + AuCR)	\$39.02	CDNS/g
Silver	NSPAq	= NSRag/NetAg	\$0.649	CDNS/g
Moly	NSPMo	= NSRMo/NetMo	\$9.70	CDNS/lb
NSR = RCU*22.046*2.93+RALP*39.04+RAG*0.649+RMO/1000*22.046*9.70				

Pit Optimization Net Smelter Price Comparison	2011 PFS	2012 PFS Update before Smelter Schedule Update	Diff	Var
Copper	\$2,684	\$2,94	\$0,255	10%
Gold	\$31.60	\$39.3	\$7.656	24%
Silver	\$0,437	\$0,658	\$0,221	51%
Moly	\$10,79	\$9,70	-\$1,091	-10%

Salaried Positions

POSITION	Base Salary	Payroll Burden	Salary With Burden
MINE OPERATIONS			
Operations General Foreman	\$115 000	45%	\$166 750
Shift Foreman	\$105 000	45%	\$152 250
Area Foreman	\$90 000	45%	\$130 500
Training General Foreman	\$90 000	45%	\$130 500
Shift Trainers	\$80 000	45%	\$116 000
Drilling & Blasting Foreman	\$105 000	45%	\$152 250
Maintenance General Foreman	\$115 000	45%	\$166 750
Maintenance Planner	\$80 000	45%	\$116 000
Maintenance Planning Clerk	\$51 000	45%	\$ 73 950
Maintenance Shift Foreman	\$105 000	45%	\$152 250
Mechanical Foreman	\$90 000	45%	\$130 500
Electrical Foreman	\$90 000	45%	\$130 500
Services Foreman	\$90 000	45%	\$130 500
Administration Assitant	\$55 000	45%	\$ 79 750
Mining Superintendent	\$150 000	45%	\$217 500
TECHNICAL SERVICES			
Senior Geologist	\$110 000	45%	\$159 500
Pit Geologist	\$70 000	45%	\$101 500
Ore Grade Technicians	\$60 000	45%	\$ 87 000
Project Engineer	\$90 000	45%	\$130 500
Senior Environmental Engineer			
Environmental Technician			
Senior Mining Engineer	\$110 000	45%	\$159 500
Mine Engineer	\$85 000	45%	\$123 250
Drilling & Blasting Engineer	\$85 000	45%	\$123 250
Drilling & Blasting Technician	\$60 000	45%	\$ 87 000
Surveyor	\$60 000	45%	\$ 87 000
Senior Surveyor	\$70 000	45%	\$101 500
Engineering Clerk	\$60 000	45%	\$ 87 000
Dispatch Engineer	\$75 550	45%	\$109 548
Senior Geotechnical Engineer	\$110 000	45%	\$159 500
-> Dispatchers			
Chief Engineer	\$125 000	45%	\$181 250

Values used in MMTS report are based on 2011 values

(covered in other part of org chart)

(covered in other part of org chart)

(Not in J Huang's List)

(make sure this is added to cost model GME)

Hourly Labour Rates

Position	Base Rate \$/hr	(Burden) %	\$/ManHr worked
MINE OPERATIONS			
Drill Operator	\$31.2	45%	45.24
Blasters	\$31.2	45%	45.24
Shovel Operator	\$32.2	45%	46.69
Haul Truck Driver	\$29.1	45%	42.20
Grader Operator	\$30.2	45%	43.79
Excavator Operator	\$30.2	45%	43.79
Loader Operator	\$31.2	45%	45.24
Track Dozer Operator	\$30.2	45%	43.79
Scraper Operator	\$29.1	45%	42.20
Crusher Operator	\$29.1	45%	42.20
Water Truck Operator	\$29.1	45%	42.20
Fuel Truck Operator	\$29.1	45%	42.20
MINE MAINTENANCE			
Electrician	\$36.5	45%	52.93
HD Mechanic	\$36.5	45%	52.93
LD Mechanic	\$33.0	45%	47.85
Machinist	\$36.5	45%	52.93
Crane Operator	\$29.1	45%	42.20
Welder	\$36.5	45%	52.93
Tireman	\$32.2	45%	46.69
Labourer Service man	\$25.0	45%	36.25

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MINE DESIGN BASIS - KSM PFS UPDATE 2012



ECONOMIC PIT LIMITS

MS-EP Costs	Waste		Ore		Waste \$/t	Ore \$/t
	Haul min		Haul min			
Mitchell	28		18		1.83	1.55
Kerr	22		22		1.66	1.66
Sulphurets	34		30		2.00	1.89
Iron Cap	30		34		1.89	2.00

M4 mid point between top and rim
mid between rim and bottom
mid between rim and top

MMTS - February 2012

Process, G&A, Tailings Treatment, Site Services and Water Treatment Costs (NSR cut-off grade)

Mitchell	9.57	\$/t ore
Sulphurets	10.17	\$/t ore
Kerr	9.61	\$/t ore
Iron Cap	9.57	\$/t ore

Pit#	CASE	Net Price for Mine, Plant, & O/H			
		Copper \$/lb	Gold \$/g	Silver \$/g	Moly \$/lb
1	30.0%	\$0.88	\$11.7	\$0.195	\$2.91
2	35.0%	\$1.03	\$13.7	\$0.227	\$3.39
3	40.0%	\$1.17	\$15.6	\$0.260	\$3.88
4	45.0%	\$1.32	\$17.6	\$0.292	\$4.36
5	50.0%	\$1.46	\$19.5	\$0.325	\$4.85
6	55.0%	\$1.61	\$21.5	\$0.357	\$5.33
7	60.0%	\$1.76	\$23.4	\$0.390	\$5.82
8	65.0%	\$1.90	\$25.4	\$0.422	\$6.30
9	70.0%	\$2.05	\$27.3	\$0.454	\$6.79
10	75.0%	\$2.20	\$29.3	\$0.487	\$7.27
11	80.0%	\$2.34	\$31.2	\$0.519	\$7.76
12	85.0%	\$2.49	\$33.2	\$0.552	\$8.24
13	90.0%	\$2.64	\$35.1	\$0.584	\$8.73
14	95.0%	\$2.78	\$37.1	\$0.617	\$9.21
15	100.0%	\$2.93	\$39.0	\$0.649	\$9.70
16	105.0%	\$3.08	\$41.0	\$0.682	\$10.18
17	110.0%	\$3.22	\$42.9	\$0.714	\$10.67
18	115.0%	\$3.37	\$44.9	\$0.747	\$11.15
19	120.0%	\$3.52	\$46.8	\$0.779	\$11.64
20	125.0%	\$3.66	\$48.8	\$0.812	\$12.12
21	130.0%	\$3.81	\$50.7	\$0.844	\$12.61
22	135.0%	\$3.96	\$52.7	\$0.877	\$13.09
23	140.0%	\$4.10	\$54.6	\$0.909	\$13.58
24	145.0%	\$4.25	\$56.6	\$0.941	\$14.06
25	150.0%	\$4.39	\$58.5	\$0.974	\$14.55

ksmp13.m1 Mitchell (base case - MI only)
ksmp13.m2 Iron Cap (base case - MI only)
ksmp13.m3 Sulphurets (base case - MI only)
ksmp13.m4 Kerr (base case - MI only)

ksmp13.m5 Mitchell (MI blocks included)
ksmp13.m6 Iron Cap (MI blocks included)
ksmp13.m7 Sulphurets (MI blocks included)
ksmp13.m8 Kerr (MI blocks included)

ksmp13.m9 Mitchell (pit slopes -5 degrees)
ksmp13.m10 Iron Cap (pit slopes -5 degrees)
ksmp13.m11 Sulphurets (pit slopes -5 degrees)
ksmp13.m12 Kerr (pit slopes -5 degrees)

ksmp13.m13 Mitchell (pit slopes +5 degrees)
ksmp13.m14 Iron Cap (pit slopes +5 degrees)
ksmp13.m15 Sulphurets (pit slopes +5 degrees)
ksmp13.m16 Kerr (pit slopes +5 degrees)

MMTS - Tracey (Feb 9, 2012)

reviewed by Jesse Aarsen on Apr 29 2012

Results are in KSM LG Pits 09 Feb 2012.xlsm

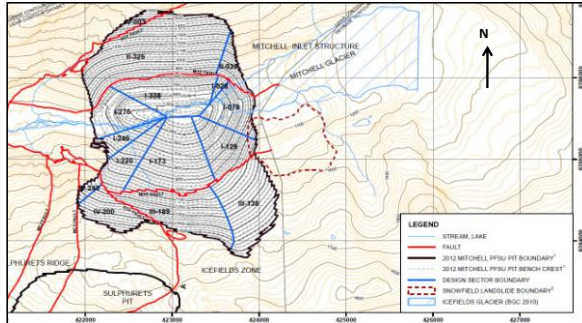
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MINE DESIGN BASIS - KSM PFS UPDATE 2012



PIT SLOPE ANGLES

Mitchell

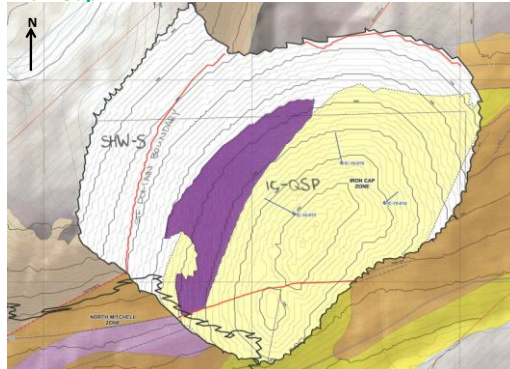


file: "20110222 DRAFT Mitchell Design Parameters rev2.pdf"
BGC (Derek Kinakin) - Feb 23, 2011

IRA Item	Domain	Azimuth start	Azimuth end	Iba degrees	Oa degrees	LG SLOPE
3	I-173	135	210	36	36	34.5
3	I-220	210	230	40	40	38
3	I-240	230	250	48	48	45
3	I-275	250	300	53	53	50
3	I-338	300	015	53	46	44
3	I-028	015	040	53	46	44
3	I-078	040	115	48	48	46
3	I-125	115	135	46	45	43
2	II-325	270	020	53	44	44
2	II-035	020	050	46	47	46
2	II-058	050	055	40	42	40
2	II-078	065	090	36	41	36
2	III-099	090	108	54	55	54
2	III-138	108	168	34	35	34
2	III-189	168	210	46	47	46
1	IV-168	145	190	46	47	46
1	IV-200	190	210	39	40	39
1	IV-240	210	270	34	36	34
1	IV-003	325	040	46	47	46

Domain	Description
I	Below Mitchell fault
II	Between Mitchell and Sulphurets fault, north side of Mitchell pit
III	Between Mitchell and Sulphurets fault, south side of Mitchell pit
IV	Above Sulphurets fault

Iron Cap

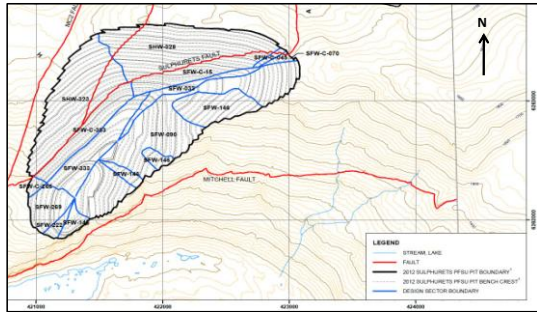


file: "IRON CAP Design Criteria 20110210 Double Bench DRAFT.pdf"
BGC (Derek Kinakin) - Feb 14, 2011

IRA Item	Domain	Design Sector	Azimuth start	Azimuth end	Iba degrees	Oa degrees	LG SLOPE
5	IC-QSP	IC-QSP-182	165	198	37	40	34
5		IC-QSP-214	198	230	50	50	47
5		IC-QSP-263	230	295	40	41	37
5		IC-QSP-310	295	325	50	49	46
5		IC-QSP-335	325	345	40	41	37
5		IC-QSP-353	345	000	36	37	36
5		IC-QSP-028	000	055	34	35	34
5		IC-QSP-110	055	165	34	35	34
4	SHW-S	SHW-S-315	270	000	44	46	44

BGC recommends 45 degrees when mining through ice

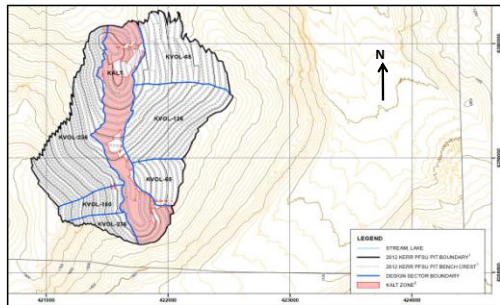
Sulphurets



file: "20110211 DRAFT SULPHURETS Design Criteria.pdf"
BGC (Derek Knakin) - Feb 14, 2011

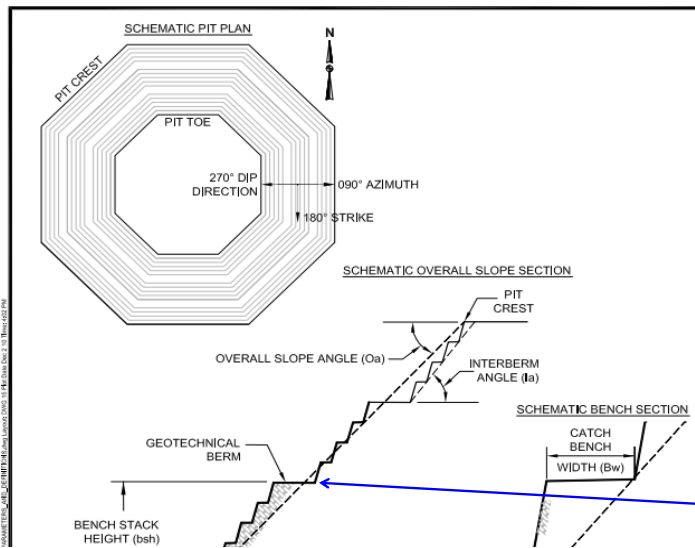
Sulphurets Pit Slope Angles							
IRA item	Domain	Design Sector	Azimuth start	Azimuth end	I _{ba} degrees	O _a degrees	LG SLOPE
6	SHW-V	SHW-V-280	270	290	49	50	46
6		SHW-V-323	290	355	40	42	37
6		SHW-V-028	355	060	45	45	42
6		SHW-V-075	060	090	36	41	36
7	SFW-C	SFW-C-265	220	310	45	49	45
7		SFW-C-333	310	355	49	53	49
7		SFW-C-015	355	035	50	53	50
7		SFW-C-045	035	055	45	49	45
7		SFW-C-070	055	085	40	45	40
8	SFW-V	SFW-V-190	172	207	40	44	37
8		SFW-V-222	207	237	47	50	44
8		SFW-V-269	237	300	37	41	35
8		SFW-V-333	300	005	40	44	37
8		SFW-V-033	005	060	36	37	34
8		SFW-V-090	060	120	40	41	38
8		SFW-V-146	120	172	36	40	34

Kerr



BGC (Derek Knakin) - Feb 15, 2011

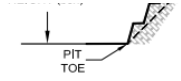
IRA item	Domain	Design Sector	Azimuth start	Azimuth end	I _{ba} degrees	O _a degrees	LG SLOPE
9	KVOL	KVOL-236	180	292	50	49	46
9		KVOL-335	292	017	36	37	34
9		KVOL-065	017	112	34	36	34
9		KVOL-126	112	140	40	41	37
9		KVOL-160	140	180	45	45	41
10	KALT	KALT-180	135	225	36	25	25
10		KALT-000	225	135	36	40	34



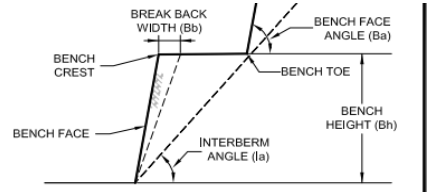
file: "20101206 GEOMETRY PARAMETERS AND DEFINITIONS.pdf"
BGC (Derek Knakin) - Dec 07, 2010

For ALL pits, a geotechnical berm is required every 150m in elevation (minimum 20m wide)

DATE: 01/11/2012 10:48:00 AM BY: J. MITCHELL

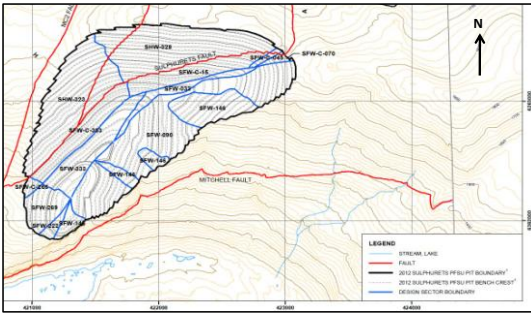


DRAFT



Sulphurets

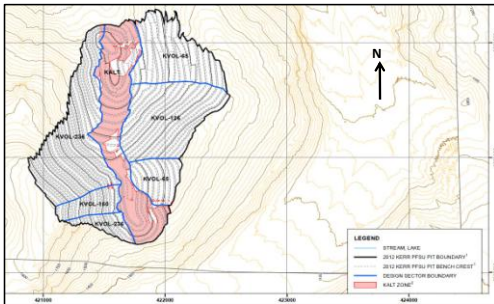
file: "20110211 DRAFT SULPHURETS Design Criteria.pdf"
BGC (Derek Kinakin) - Feb 14, 2011



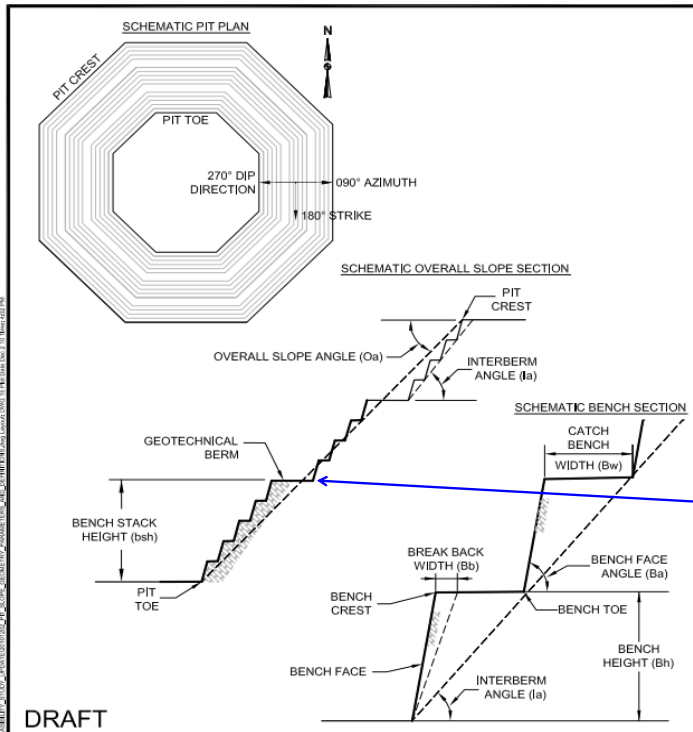
Sulphurets Pit Slope Angles							
IRA Item	Domain	Design Sector	Azimuth start	Azimuth end	Iba degrees	Oa degrees	LG SLOPE
6	SHW-V	SHW-V-280	270	290	49	50	46
6		SHW-V-323	290	355	40	42	37
6		SHW-V-028	355	060	45	45	42
6		SHW-V-075	060	090	36	41	36
7	SFW-C	SFW-C-265	220	310	45	49	45
7		SFW-C-333	310	355	49	53	49
7		SFW-C-015	355	035	50	53	50
7		SFW-C-045	035	055	45	49	45
7		SFW-C-070	055	085	40	45	40
8	SFW-V	SFW-V-190	172	207	40	44	37
8		SFW-V-222	207	237	47	50	44
8		SFW-V-269	237	300	37	41	35
8		SFW-V-333	300	005	40	44	37
8		SFW-V-080	005	060	36	37	34
8		SFW-V-146	120	172	36	40	34

Kerr

BGC (Derek Kinakin) - Feb 15, 2011



IRA Item	Domain	Design Sector	Azimuth start	Azimuth end	Iba degrees	Oa degrees	LG SLOPE
9	KVOL	KVOL-236	180	292	50	49	46
9		KVOL-335	292	017	36	37	34
9		KVOL-065	017	112	34	36	34
9		KVOL-126	112	140	40	41	37
9		KVOL-180	140	180	45	45	41
10	KALT	KALT-180	135	225	36	25	25
10		KALT-000	225	135	36	40	34



file: "20101206 GEOMETRY PARAMETERS AND DEFINITIONS.pdf"
BGC (Derek Kinakin) - Dec 07, 2010

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MINE DESIGN BASIS - KSM PFS UPDATE 2012

PIT SLOPE MATRIX (from wall azimuth) - lba values from BGC

All Pits

BGC Domain or domain description	ksmp15.dat IRA value	Azimuth																																													
		0	5	17	20	35	40	50	55	60	65	108	112	115	120	135	140	165	168	172	180	190	198	207	210	220	225	230	237	250	270	280	290	292	295	300	310	325	345	355							
Above STF (IV)	1	46																			42	39			34						34																
Between STF and MTF (II and III)	2	44			46			40									40	46							40			44	48		52						46										
Below MTF (I)	3	46												45	42	36																															
IC above STF (SHW-S)	4	44																																													
IC below STF (IC-QSP)	5	34																37																													
SHW-V	6	45							40	36																																					
SFW-C	7	50				45			40																																						
SFW-V	8	40	36												36																																
KVOL	9	36		34									40																																		
KALT	10	36													30	25																															

BENCH FACE MATRIX (from wall azimuth) - Ba values from BGC

All Pits

BGC Domain or domain description	ksmp15.dat IRA value	Azimuth		
		0	115	210
Above STF (IV)	1	70		
Between STF and MTF (II and III)	2	70		
Below MTF (I)	3	70	60	70
IC above STF (SHW-S)	4	65		
IC below STF (IC-QSP)	5	65		
SHW-V	6	65		
SFW-C	7	65		
SFW-V	8	65		
KVOL	9	65		
KALT	10	60		

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MINE DESIGN BASIS - KSM PFS UPDATE 2012

2012

RESERVE/RESOURCE ESTIMATION

Pit Delineated Reserve Calculation - Using MineSight PITRES and GNDLN routines

MINING RECOVERY

MITCHELL
SULPHURETS
KERR

		TOTAL LOSS	
	97.8%	2.2%	Feb 15, 2012 MMTS calculation (JA)
	94.7%	5.3%	Feb 15, 2012 MMTS calculation (JA)
	95.5%	4.5%	Feb 15, 2012 MMTS calculation (JA)

WHOLE BLOCK DILUTION

MITCHELL
SULPHURETS
KERR

	0.8%		Feb 15, 2012 MMTS calculation (JA)
	3.9%		Feb 15, 2012 MMTS calculation (JA)
	3.2%		Feb 15, 2012 MMTS calculation (JA)

Loss and Dilution calculations on FTP

Cut-Off Grade - NSR

MITCHELL + IC
SULPHURETS
KERR

	9.57	\$/t	from Wardrop process costs
	10.17	\$/t	from Wardrop process costs
	9.61	\$/t	from Wardrop process costs

Default SG:

MITCHELL
SULPHURETS
KERR
IRON CAP

	2.78	t/m ³	pitres run on Feb 22, 2011
	2.77	t/m ³	pitres run on Feb 22, 2011
	2.85	t/m ³	pitres run on Feb 22, 2011
	2.74	t/m ³	pitres run on Feb 22, 2011

$$NSR = RCU * 22.046 * 2.93 + RAU * 39.02 + RAG * 0.649 + RMO / 10000 * 22.046 * 9.7$$

updated from 2012 metal prices

Ore NSR Cut off

COG (covers process)	9.57	\$/t ore
Sub grade (Covers milling plus S/P R/H + 20% rec loss)	11.48	\$/t ore
Mid Grade (Covers milling + mining costs + 10% premium) rounded up	11.00	\$/t ore
High Grade 1	14.00	\$/t ore
High Grade 2	16.00	\$/t ore
High Grade 3	18.00	\$/t ore
High Grade 4	20.00	\$/t ore
High Grade 5	24.00	\$/t ore
High Grade 6	28.00	\$/t ore
Based on:		
Mining		\$/t ore
Process	9.568	\$/t ore
Stockpile rehandle		\$/t ore

Dilution Grades

	5<NSR<9.57	5<NSR<10.17	5<NSR<9.61
	M685	Sulphurets PIT13	Kerr PIT13
output file	mdlh.rpt	sdllh.rpt	kdllh.rpt
NSR	7.55	8.19	7.60
CUIDW	0.043	0.056	0.106
AUIDW	0.229	0.333	0.141
RCU	0.021	0.028	0.069
RAU	0.136	0.160	0.077
AGIDW	1.45	0.59	0.78
MOIDW	59.4	19.0	0.0
RAG	0.67	0.18	0.24
RMO	20.6	3.3	0.0

MMTS pitres runs on Feb 15, 2012 (checked by JA)

PFS Reserves Based on Mitchell Series 8 Pits and Kerr, Sulphurets Series 9 in "KSM RESERVE 19 April 2012.xlsx"

Area	Ore (mt)	Diluted Grades					Waste (mt)	S/R (t:t)
		NSR (Cdn\$/t)	Au (g/t)	Cu (%)	Ag (g/t)	Mo (ppm)		
Mitchell Pit								
M681	88	39.7	0.839	0.227	3.40	24.6	67	0.8
M682i	239	31.4	0.689	0.177	2.58	64.0	423	1.8
M683i	116	28.9	0.643	0.155	3.38	53.0	287	2.5
M684i	209	24.3	0.544	0.136	2.34	86.4	257	1.2
M685i	322	28.2	0.618	0.157	3.24	62.3	486	1.5
Subtotal	973	29.3	0.642	0.163	2.92	63.4	1 519	1.6
Kerr Pit								
K691	242	30.6	0.244	0.454	1.20	0.0	665	2.7
Sulphurets Pit								
S691	101	31.4	0.654	0.261	0.59	54.9	167	1.7
S692i	217	25.0	0.553	0.200	0.88	48.6	683	3.2
Subtotal	318	27.0	0.585	0.219	0.79	50.6	850	2.7
Subtotal Pit	1 533	29.0	0.567	0.221	2.20	50.7	3 035	2.0
Underground Mining								
Mitchell	438	26.4	0.529	0.165	3.48	33.6	-	-
Iron Cap	193	25.3	0.450	0.196	5.32	21.5	-	-
Subtotal	631	26.1	0.505	0.174	4.05	29.9	-	-
Grand Total	2 164	28.1	0.549	0.207	2.74	44.7	3 035	1.4

Check files on FTP

MineSight Files

out .rpt .scd

M1	M1
M2	M2i
M3	M3i
M4	M4i
M5	M5i
K1	K1
S1	S1
S2	S2i

Seabridge Gold Inc.

MINE DESIGN BASIS - KSM PFS UPDATE 2012



PIT DESIGN

Equipment Fleet

Major Mining Fleet

Shovels 100 tonne dipper cable shovels (P&H 4100)
Trucks 345 tonne truck (CAT 797)

Drills Primary = 12 1/4 inch electric drill (P&H 120A)
 high wall = 150 mm diesel - (Sandvick D2455)

Equipment Selection

Bunching Maximum (dependant on fleet match)	15%		CAT
Shift eff for tkph calc	75%		CAT
TKPH limit (797 59/80R63)	2218		Michelin XDR C4
Fleet Matching factor	<1		MMTS
Minimum 3 passes to load a truck.			
Max pit ramp slope	8%		For winter conditions
Min haul road radius	75	m	CAT Handbook
Waste Dump Angle of Repose	37°		Blasted rock
Largest Vehicle Overall Width (CAT 797B)	9.8	m	CAT 797 Spec
Maximum Tire Height (59/80R63)	4.0	m	Michelin
Minimum Haul road outside berm height	3.0	m	Mines Act based on tire height
Minimum Shoulder / Berm Width	8.9	m	

<u>Double lane highwall haul road allowance</u>	38.2	m	BC Mines Act
<u>Double lane external haul road allowance</u>	47.2	m	BC Mines Act
<u>Single lane highwall haul road allowance</u>	28.5	m	BC Mines Act
<u>Single lane external haul road allowance</u>	37.4	m	BC Mines Act
Runaway lanes or retardation barriers where conditions/risk warrant on roadways where			BC Mines Act
Speed Limits Around Corners	40.00	kph	CAT Handbook

Last bench will not need haul road. Temporary internal ramps will be used
 Last 2 haul benches have single lane haul roads
 Minimum pit base width is shovel operating width. 50 m JA estimate, Jan 2011

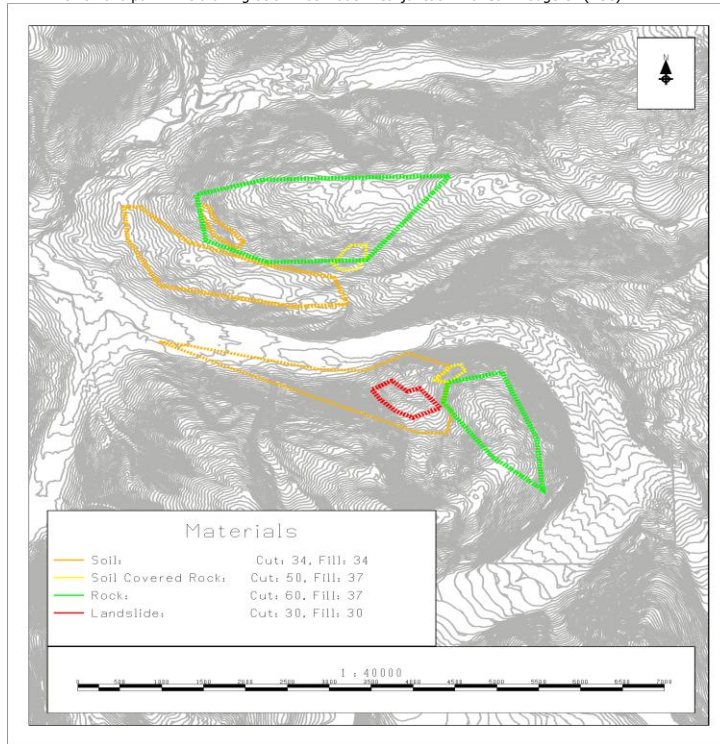
	# of lanes	Grade
Main Ramp	2	8%
Last 2 benches of Ramp	1	8%
Last 2 benches of Pit Phase	No ramp	

Current Road Series **Series 8 - 5**

msr objects built by Jesse, Feb 2012 and Matt in Apr 2012
 Added January 4 2011

Sulphurets Valley Design Criteria

Based on "KSM_MineSiteRoads_Draft.pdf", and "Summary of Geotech Cut Fill Prescriptions Nov 8 2010.pdf". The drawing below was made in conjunction with Sam Fougeren (BGC).



Mitchell Valley North Design Criteria			added October 13, 2010
Cuts under 30m high	60 Degrees		BGC (Sept 2010)
Cuts over 30m high	50 Degrees		
MSE fill	85 Degrees	Must be less than 25m high	

Road Design (External to pit, Non-Haul Road)				added March 3, 2010
	Lanes	Width	Max Grade	Description
Type I	2	20	10%	Well traveled, main access roads: all vehicles, can accommodate limited un-loaded haul truck access
Type II	1	10	10%	Light traveled, main access roads: light trucks, tractor trailers, and service vehicles
Type III	1	12	15%	Infrastructure service roads: pick-up trucks and service/parts vehicles, tractor trailers may require chains
Type IV	1	6	15%	Remote facility access road: pick-up trucks
Type V	1	10	15%	Pioneering road: limited use, construction equipment

Berms		received in email from Derek Kinakin (BGC) on Dec 7, 2010
20m berm every 5 double benches (150m) vertical height (as recommended to BGC by Pete Stacey)		

Waste Dump Engineering			Based on Rescan's "KSM RSF Closure Criteria Memo 21JAN11.pdf"
Natural angle of repose		37°	Updated January 4, 2011
Maximum free dumping height		300 m	
Dumped waste swell factor		1.2	
Reclaimed dump slopes		26°	
Type A: Reclaimed Slopes			
<ul style="list-style-type: none"> Approximately 3m service roads will be built in the slope every 30m vertically (insignificant effect on overall slope) Dump face angle (26 Deg.) Overall slope angle (26 Deg.) Cover will be placed on entire slope 			
Type B: Reclaimed Flats Only			
<ul style="list-style-type: none"> Flat benches will be provided at 15m vertical intervals Dump face angle (37 Deg) Overall slope angle (26 Deg) Cover will be placed on flat benches only 			
McTagg RSF			
Below 1100m	Overall Slope	26°	
	Reclamation	Type A or B	
Above 1100m	Face Slope	37°	
	Overall Slope	37° plus ramps and 3m benches	
	Reclamation	none	
	Maximum 50m vertical interval of continuous slope		
Mitchell RSF			
Below 840m	Overall Slope	26°	
	Reclamation	Type A or B	
Above 840m	Face Slope	37°	
	Overall Slope	26°	
	Reclamation	Till on flats up to 1100m elev.	
	Maximum 50m vertical interval of continuous slope (50m lift heights)		
Sulphurets RSF			
Below 1100m (entire RSF)	Overall Slope	26°	
	Reclamation	Type A or B	

Production Drilling and Blasting			
Drilling - Primary Drill (P&H 120A)			
Pattern - m2 (8.5m square equivalent)	72.25 m2		from Orica Sabrex report
SG - t/m3	2.77 t/m3		
Bench Height - m	15 m		
Yield (t/hole)	3 002 t/hole		
Sub-drill	2 m		from Orica Sabrex report
Penetration Rate - m/hr	25 m/hr		estimation (based on other studies and actual numbers)
Hole depth	17 m		
Setup Time - minutes	2.0 min		
Drill Time - minutes	40.5 min		
Move Time - minutes	2.0 min		
Total Cycle Time - minutes	44.5 min		
Holes per Hour	1.35		
Blasting			
Spacing / Burden	8.5 m		from Orica Sabrex report
Hole Size	311 mm		from Orica Sabrex report
Explosive In-Hole Density	12.25 inch hole		
	1.25 g/cc		from Orica Sabrex report
	95.0 kg/m		
Bench Height	15 m		
Sub-drill	2.0 m		from Orica Sabrex report
Collar	6 m		from Orica Sabrex report
Charge per hole	1046 kg/hole		
Tons per hole	3 002 t/hole		
Powder factor	0.35 kg/t		from Orica Sabrex report
	0.97 kg/m3		
% ANFO	0.30		from Orica Sabrex report
Bulk Explosive - \$/ kg	\$ 0.70	\$/kg	
Initiation Systems - \$/ hole	\$ 15.55	\$/hole	"Seabridge Gold Operation with capital costs October 2009.doc"
Booster - \$ each	\$ 6.50	\$ each	"Seabridge Gold Operation with capital costs October 2009.doc"
highwall hole spacing	1.80 m		"KSM - Mitchell Pit - Wall Control PFS.xls"

No drilling and blasting differentiation between rocktypes

Seabridge Gold Inc.

MINE DESIGN BASIS - KSM PFS UPDATE 2012



SCHEDULING

A Minimum mill feed Cu grade of 0.15% is required

Phase Names

M681	Mitchell starter pit
M682	Incremental pushback to the south
M683	First mining phase on the north side
M684	Incremental pushback to south final limits
M685	Pushback to north final limits - Mitchell ultimate open pit (1200m highwall)
S691	Sulphurets starter pit
S692	Sulphurets final pit
K691	Kerr ultimate pit

Times

Spot & Dump Time	0.5	min
Delay Time	1.0	min
Truck Factor	363	Tonne per load
Haul Cycles		
Rolling Resistance In Pit	5	%
Rolling Resistance On Ramp	3	%
Rolling Resistance Haul Road	3	%
Rolling Resistance On Dump	8	%

Loading Time

PFS Production Schedule

Shovel	Truck	Cycle Time	# Passes	Job	Spot and Wait	Operating	Utilization	MS-SP	MS-SP	Productivity
		per pass		Efficiency	time per load	Efficiency	Efficiency	Loading Time	Efficiency	
		sec		%	sec	%	%	min / load	factor	tonnes/ ophr
RH400 85t	CAT 797	35	4	84%	10	80%	96%	2.94	80%	5918
P&H 4100 104t	CAT 797	35	4	84%	10	80%	96%	2.94	80%	5918
EX3500	CAT 797	35	7	84%	10	80%	96%	5.03	80%	3466

Truck Haul Times

Spot & Dump Time	1.5	min	MMTS Estimate
Truck Operating Efficiency (to MSSP)	83%		MMTS Estimate
Truck Factor Waste and ORE	363	tonne per load	CAT spec
Haul Cycles			
Rolling Resistance In Pit	5	%	MMTS Estimate
Rolling Resistance On Ramp	3	%	MMTS Estimate
Rolling Resistance Haul Road	3	%	MMTS Estimate
Rolling Resistance On Dump	5	%	MMTS Estimate
Haul Operator Efficiency	90%		MMTS Estimate
Max speed	50 km/h		MMTS Estimate

Weather Studies

MEMORANDUM

To: Jim Gray, GR Technical Services
 From: W. Scott Dunbar
 Date: May 20, 2010
 Subject: Simulation of KSM Storm Production Scenarios

Table 2
Results of Simulation

Expected Hours at Each Level during Storm Season	Level 2	Level 3	Level 4	Level 5
Average (hrs)	47.4	84.6	55.8	26.2
Standard deviation (hrs)	0.9	8.5	14.9	13.6

Operation Level	Duration D (hrs)	Description
L1	na	Normal snow season operation (derated for snow)
L2	D ≤ 6	5 shovels, 2 scrapers, 2 graders
L3	6 < D ≤ 12	4 shovels, 4 scrapers
L4	12 < D ≤ 18	2 shovels, 6 scrapers
L5	D > 18	0 shovels (full pit shutdown, mill fed from stockpile)

For a 5 Shovel Operation

Visibility less than 1 km days	4.75	Days	Rescan Memo :11/19/2010
Days down required for Extreme Weather (Level 5)	1.5	Days	
time at level 4	55.8	Hours	
time at level 3	84.6	Hours	
time at level 2	47.4	Hours	
Mine Load And Haul Utilization adjustment at Level 4	40%		
Mine Load And Haul Utilization adjustment at Level 3	60%		
Mine Load And Haul Utilization adjustment at Level 2	80%		
Weighted Lost hours Adjustment for Extreme Weather L2 to L4	-76.8		
Weighted Utilization Adjustment for Extreme Weather L2 to L4	-1.0%		(TM: I allowed an -3% reduction in the cost model)

Waste classification

(values imported into ksmpr15.dat)

SNPRA	Label	ABA
0-1,2	PAG	1
1,2,2	Unobtain	2
2+	NAG	3
	Ice	4 (coded from BGC and KCB ice solids)
	Rehandle	5

Updated by ME based on April 2 2012 report received file "06-04-10 KSM ABA Model-CSV.zip" from Mike Lechner
 ABA model was generated on April 2, 2012

PRODUCTION AND LABOUR ASSUMPTIONS

Crews	4
Shifts per Day	2
Hours per Shift	12
Calendar days per year	365
Non scheduled days (shut downs, weather etc.)	5
Scheduled working days per year	360
Total Mine Calendar Hours	8 640
Shift Utilisation (10.5/12)	0.875
Scheduled working hours	7560
Efficiency (50 min hours)	0.83
Based on two 12 hr shifts/day, 7 days/week	

Plans Construction fill from material with SNPRA > 1.9. (From Borrow Pit)

Waste Needed for Waster Storage Dam during PP :

6.5 Mm3 of random rockfill and 0.7 Mm3 of non acid reactive (ie intrusive) rockfill, 1.4 Mm3 of competent angular rock fill.

Table 8.1 Borrow Materials Required for Construction of Ultimate WSD

Zone	Material	To 706 m ³ (Km ³)	To 716 m ³ (Km ³)*	Source
1	Random Rockfill	5 674	912	Pit run of nearby quarrying or impoundment area quarry. Mine prestripping rock is also a potential source of rockfill.
2	Non Reactive (NR) Rockfill	597	96	Select quarried rock (intrusives or phyllites)
3	Clean Rockfill	1 194	192	Select free draining coarse rockfill
4	Drain	337	-	Screened alluvial sands and gravels – Ted Morris Valley
5	Non- Reactive (NR) Filter /Transition	225	15	Screened alluvial material or crushed intrusives
6	Random Moraine Central Earth Zone	1 528	73	Moraine area at McTagg- Mitchell confluence
7	Aggregate for Asphalt Core Zones	44.2	4.2	Screened moraine material
	SubTotals	9 599	1 292	
	Total Fill	10 891		

* Additional volume to raise to 716 m

drillhole file: ksmpp1.012
 3d surface model: ksmpp13.011
 3d block model: ksmpp15.dat

ksmpp15.dat

ITEM	MIN	MAX	PREC	Description
TOPO	0	100	1	percentage of the block that is below topography
SG	0	5.09	0.01	SG t/m3
AUIDW	0	8.19	0.001	Au grade g/t
CUIDW	0	2.05	0.001	Cu grade %
MOIDW	0	2045	1	Mo Grade ppm
AGIDW	0	409.3	0.1	Ag grade g/t
LITH	0	29	1	Lithologic Code
AREA	0	5	1	provided by Mike Lechner (1=Kerr, 2=Sulphurets, 3=Mitchell, 4=Iron Cap)
FAULT	0	5	1	(Not loaded)
CLASS	0	5	1	Class 1= measured, 2 = indicated, 3 = inferred
ORTYP	0	29	1	provided by Mike Lechner (codes outlined in table below)
AUREC	0	100	0.1	Au recovery %
CUREC	0	100	0.1	Cu recovery %
MOREC	0	100	0.1	Mo recovery %
AGREC	0	100	0.1	Ag recovery %
RAU	0	8.19	0.001	Au recovered grade g/t
RCU	0	2.05	0.001	Cu recovered grade %
RMO	0	2045	1	Mo recovered Grade ppm
RAG	0	410	0.1	Ag recovered grade g/t
NSR	0	500	0.01	NSR \$/t
IRA	0	90	1	Inter ramp angle code (see pit slope sheet)
BFA	0	90	0.1	Bench Face angle code (see pit slope sheet)
SNPRA	0	200	0.1	Neutralizing potential, imported into model from Jun 4, 2010 and file provided by Mike Lechner (will be updated mid February 2012)
ABA	0	5	1	1=PAG, 2=Uncertain, 3=NPAG, 4=Ice, 5=Rehandle (will be updated mid February 2012)
ROCK	0	200	1	(Used to distinguish rock type and ABA data, see table below)
ALTER	0	100	1	Alteration Code (not loaded)
SPABA	0	100	0.1	
CLAS1	0	1000	0.1	
REHAN	0	100	0.001	
MABA	0	100	1	Mitchell ABA
KABA	0	100	1	Kerr ABA
SABA	0	100	1	Sulphure ABA
IABA	0	100	1	Iron Cap ABA
RESCA	0	10000	0.01	Used to find ABA values of the pit surface
RATE	0	1000	0.001	
AROCK	0	100	0.1	
XTRA2	0	100	0.1	
XTRA3	0	100	0.1	
NSR11	0	500	0.01	
AUEQ	0	8.19	0.001	Gold Equivalent Grade

ROCK	AROCK	Description	ABA
1	11	Kerr - overburden	SNPRA<1.2
2	12	Kerr - CL-PR	SNPRA<1.2
3	13	Kerr - QSP	SNPRA<1.2
4	14	Kerr - weak CLOSP	SNPRA<1.2
5	15	Kerr - dikes (Premier & hornblende)	SNPRA<1.2
6	19	Kerr - undefined	SNPRA<1.2
7	21	Sulphurets - overburden	SNPRA<1.2
8	22	Sulphurets - Au, leach & Raewyn zones	SNPRA<1.2
9	23	Sulphurets - lower Au zone	SNPRA<1.2
10	24	Sulphurets - lower plate Hazelton	SNPRA<1.2
11	25	Sulphurets - upper plate Hazelton	SNPRA<1.2
12	26	Sulphurets - monzonite	SNPRA<1.2
13	29	Sulphurets - undefined	SNPRA<1.2
14	31	Mitchell - overburden	SNPRA<1.2
15	32	Mitchell - glacial ice	SNPRA<1.2
16	33	Mitchell - upper plate Hazelton	SNPRA<1.2
17	34	Mitchell - lower plate Hazelton	SNPRA<1.2
18	35	Mitchell - monzonite	SNPRA<1.2
19	36	Mitchell - bornite/leach breccia	SNPRA<1.2
20	39	Mitchell - undefined	SNPRA<1.2
21	41	Iron Cap - overburden	SNPRA<1.2
22	42	Iron Cap - glacial ice	SNPRA<1.2
23	43	Iron Cap - Hazelton	SNPRA<1.2
24	44	Iron Cap - diorite	SNPRA<1.2
25	45	Iron Cap - monzonite	SNPRA<1.2
26	49	Iron Cap - undefined	SNPRA<1.2
27	11	Kerr - overburden	1.2<=SNPRA<2
28	12	Kerr - CL-PR	1.2<=SNPRA<2
29	13	Kerr - QSP	1.2<=SNPRA<2
30	14	Kerr - weak CLOSP	1.2<=SNPRA<2
31	15	Kerr - dikes (Premier & hornblende)	1.2<=SNPRA<2
32	19	Kerr - undefined	1.2<=SNPRA<2
33	21	Sulphurets - overburden	1.2<=SNPRA<2
34	22	Sulphurets - Au, leach & Raewyn zones	1.2<=SNPRA<2
35	23	Sulphurets - lower Au zone	1.2<=SNPRA<2
36	24	Sulphurets - lower plate Hazelton	1.2<=SNPRA<2
37	25	Sulphurets - upper plate Hazelton	1.2<=SNPRA<2
38	26	Sulphurets - monzonite	1.2<=SNPRA<2
39	29	Sulphurets - undefined	1.2<=SNPRA<2
40	31	Mitchell - overburden	1.2<=SNPRA<2
41	32	Mitchell - glacial ice	1.2<=SNPRA<2
42	33	Mitchell - upper plate Hazelton	1.2<=SNPRA<2
43	34	Mitchell - lower plate Hazelton	1.2<=SNPRA<2
44	35	Mitchell - monzonite	1.2<=SNPRA<2
45	36	Mitchell - bornite/leach breccia	1.2<=SNPRA<2
46	39	Mitchell - undefined	1.2<=SNPRA<2
47	41	Iron Cap - overburden	1.2<=SNPRA<2
48	42	Iron Cap - glacial ice	1.2<=SNPRA<2
49	43	Iron Cap - Hazelton	1.2<=SNPRA<2
50	44	Iron Cap - diorite	1.2<=SNPRA<2
51	45	Iron Cap - monzonite	1.2<=SNPRA<2
52	49	Iron Cap - undefined	1.2<=SNPRA<2
53	11	Kerr - overburden	2<=SNPRA
54	12	Kerr - CL-PR	2<=SNPRA
55	13	Kerr - QSP	2<=SNPRA
56	14	Kerr - weak CLOSP	2<=SNPRA
57	15	Kerr - dikes (Premier & hornblende)	2<=SNPRA
58	19	Kerr - undefined	2<=SNPRA
59	21	Sulphurets - overburden	2<=SNPRA
60	22	Sulphurets - Au, leach & Raewyn zones	2<=SNPRA
61	23	Sulphurets - lower Au zone	2<=SNPRA
62	24	Sulphurets - lower plate Hazelton	2<=SNPRA
63	25	Sulphurets - upper plate Hazelton	2<=SNPRA
64	26	Sulphurets - monzonite	2<=SNPRA
65	29	Sulphurets - undefined	2<=SNPRA
66	31	Mitchell - overburden	2<=SNPRA
67	32	Mitchell - glacial ice	2<=SNPRA
68	33	Mitchell - upper plate Hazelton	2<=SNPRA
69	34	Mitchell - lower plate Hazelton	2<=SNPRA
70	35	Mitchell - monzonite	2<=SNPRA
71	36	Mitchell - bornite/leach breccia	2<=SNPRA
72	39	Mitchell - undefined	2<=SNPRA
73	41	Iron Cap - overburden	2<=SNPRA
74	42	Iron Cap - glacial ice	2<=SNPRA
75	43	Iron Cap - Hazelton	2<=SNPRA
76	44	Iron Cap - diorite	2<=SNPRA
77	45	Iron Cap - monzonite	2<=SNPRA
78	49	Iron Cap - undefined	2<=SNPRA

Ore Type	
ORTYP	Description
1	Mitchell - QSP
2	Mitchell - IARG
3	Mitchell - CL-PR
4	Mitchell - High quartz
5	Mitchell - Hornfels (upper plate)
6	Mitchell - Hornfels (lower plate)
7	Monzonite - Mitchell and Sulphurets
8	Mitchell - Bornite breccia
9	Sulphurets - Gold breccia
10	Sulphurets - Gold leach breccia
11	Sulphurets - Raewyn Copper
12	Sulphurets - Hazelton volcanics
13	Sulphurets - Late mafic intrusions
14	Kerr - all material
15	Iron Cap - all material
29	Undefined