

SNC-Lavalin GEM Québec inc.
5955 Saint-Laurent Street, Suite 300 Lévis, Québec Canada G6V 3P5
418.837.3621 418.837.2039

March 24, 2016

Mrs. Mariana Trindade, Biologist, Ph.D. Groupe Hémisphères 1453 Beaubien Street East, Suite 301 Montréal, Québec H2G 3C6 Sent by email: mtrindade@hermis.ca

Subject: Technical Memorandum Hydrogeology modeling for the Howse deposit Scenarios of wet and dry years Howse Minerals Limited Our file n°: 636981

Dear Madam:

SNC-Lavalin GEM<sup>1</sup> Québec inc. (further referred to as "SNC-Lavalin Environment and Geoscience") is pleased to provide you with the hydrogeology modeling update results for the Howse deposit regarding the open pit dewatering activities.

We trust that this technical report is to your satisfaction. Do not hesitate to communicate with the undersigned should you have further questions regarding the content of this report.

Regards,

<Original signed by>

Abdelmounem Benlahcen, geo., Ph.D.

Senior Hydrogeologist

Environment and geoscience Infrastructure

AB/lh

p.j.



<sup>&</sup>lt;sup>1</sup> GEM: Géotechnique – Environnement – Matériaux

### 1 Introduction

A numerical model update for the Howse pit dewatering was conducted by SNC-Lavalin (2015) using complementary hydrogeological program conducted in the fall of 2015 by Geofor and on water balance calculation made for an average year.

To study the effect of wetter and dryer years on the water regime, two new modeling scenarios were conducted to represent these conditions. The following sections present the results of these new scenarios.

#### 2 Modeling scenarios

Accurate values of recharge at the site requires a large amount of data of several complete years of stream flow, data infiltration and runoff volumes, and hydrological modeling of one or more representative watersheds in the Howse area. Therefore, estimated recharge may vary depending on the theoretical methods and hypothesis used.

The statistic results on precipitation and evapotranspiration summarized in Table 1 show that the evapotranspiration rate is relatively higher for a dry year in comparison to a wet year, and it represents 20% of the total precipitation. If the annual recharge rate is considered to be 20% of the net water depth available as was considered in previous modeling report, it would be estimated to 85 mm and 185 mm for a dry year and a wet year respectively. For a security factor, the annual recharge rate was decreased to 15% of net water depth available (equivalent to 60 mm) for a dry year, and increased to 27% (equivalent to 250 mm) for a wet year.

	Precipitation <sup>1</sup> (mm)	Evapotranspiration (mm)	Evapotranspiration (%)	Recharge <sup>2</sup> (mm)
Average year	782	111	14%	134
Dry year	532	106	20%	85
Wet year	1041	117	11%	185

Table 1 Summary of statistic results on precipitation and evapotranspiration (from the Water Management	
Plan update report, SNC-Lavalin, 2016)	

<sup>1</sup> Precipitation includes rainfall and snowfall

<sup>2</sup> Recharge = 20% of net water depth available (Following the same method for recharge estimation in SNC-Lavalin report (2015) and Hydrogeology report of Geofor (2015))

Previous modeling of the Howse deposit included one base case scenario and sensitivity analyses by the modeling of three scenarios. The sensitivity analysis includes the increasing of the recharge and hydraulic conductivity of the hydrogeological units in the model. In case for the recharge, the scenarios were achieved by increasing the recharge from 100 to 200 mm/yr (case 2 of Table 2). For the hydraulic conductivity, it was multiplied by two for the overburden and Sokoman formation (case 5 of Table 2) and for all hydrogeological units (case 7 of Table 5).

Four new modeling scenarios are using the new recharge values for dry and wet years (Table 2). These scenarios are:

- Scenarios of cases 1 and 3 using the base case scenario and recharge values of 60 mm/yr and 250 mm/yr for a dry year and a wet year respectively;
- Scenarios of cases 4 and 6 using the base case scenario for which hydraulic conductivities for overburden and Sokoman were doubled, and recharge values of 60 mm/yr and 250 mm/yr for a dry year and a wet year respectively.

The scenarios of case 1 and 6 are considered respectively, minimal and maximal pumping scenarios for dry and wet years in the water management plan. The scenario 7 was not modeled with a recharge of 250 mm/y and was considered not representative due to the fact that the hydraulic conductivities are overestimated in this scenario.

All the scenario results are summarized in Table 2. The new scenarios' results are presented in detail in Appendix A. A graph of the recharge versus the generated flow rate is presented in Figure 1, and shows a good correlation between these two parameters. In fact, the flow rate is proportional to the recharge, and the data follow a good straight line.

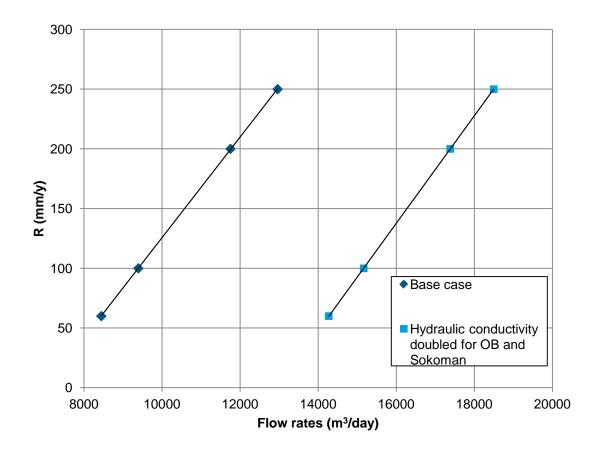
	Flow rates (m <sup>3</sup> /day)		Note (and Appendix A on consitiuity analysis for	Pumping	
Scenario	Model	Safety factor of 1.25	Note (see Appendix A on sensitivity analysis for more details)	rate increase	
Base case:	9393	11741	Kx, Ky, Kz;		
Calibrated model	9393	11741	Recharge : 100 mm/y		
Sensitivity analysis	8445		Kx, Ky, Kz;	0.0	
Case 1	0443	-	Recharge decreased to 60 mm/y	0.9	
Sensitivity analysis	11754	14602	Kx, Ky, Kz;	4.0	
Case 2	11/04	14693	Recharge increased to 200 mm/y	1.3	
Sensitivity analysis		40000	Kx, Ky, Kz;	1.4	
Case 3	12962	16203	Recharge increased to 250 mm/y	1.4	
Sensitivity analysis Case 4 14270		17838	Kx, Ky and Kz multiplied by 2 for OB and Sokoman,	1.5	
			Recharge decreased to 60 mm/y		
Sensitivity analysis Case 5			Kx, Ky and Kz multiplied by 2 for OB and Sokoman,	1.9	
Case 5			Recharge increased to 200 mm/y		
Sensitivity analysis Case 6 18497 23121		23121	Kx, Ky and Kz multiplied by 2 for OB and Sokoman,	2.0	
			Recharge increased to 250 mm/y		
Sensitivity analysis Case 7	18752 23440		Kx, Ky and Kz multiplied by 2 for all five units (OB, Sokoman, Wishart, Shale and Fault zones),	2.0	
Case /			Recharge increased to 200 mm/y		

#### Table 2 Dewatering Simulation Results

- Base case scenario and scenarios of cases 2, 5 and 7 are conducted in previous model (SNL-Lavalin, 2015).

- Scenarios of cases 1, 3, 4 and 6 are new scenarios for which the results are presented in details in Appendix A

- Highlighted in bold are flow rates considered for dry, average and wet years for the Water Management Plan.



# Figure 1 Simulated Recharge and Dewatering Rate Results (Kx, Ky and Kz of base case scenario are maintained constant)

### 3 Conclusions

The current groundwater flow modeling has allowed for the evaluation of dewatering flow rates of the Howse deposit for a dry year and a wet year. The main conclusions from the modeling results are:

For a dry year scenario with a recharge of 60 mm, the estimated dewatering rate is about 8,500 m<sup>3</sup>/day;

For a wet year scenario with a recharge of 250 mm and conductivity hydraulic multiplied by 2 for overburden and Sokoman units, the estimated dewatering rate is about 23,200 m<sup>3</sup>/day.

<Original signed by>

<Original signed by>

Abdelmounem Benlahcen, geo., Ph.D. Senior Hydrogeologist Environment and geoscience Infrastructure Christian Bélanger, Eng., M.Sc.A. Senior Hydrogeologist Environment and geoscience Infrastructure

#### References

Geofor Environnement, November 2015. 2015's Hydrogeological Campaign results on Howse deposit. Hydrogeology chapter of the EIA Howse property project report.

SNC-Lavalin (2015). Hydrogeology Numerical Modeling for the Howse Deposit – Update. Howse Property Project. Howse Minerals Limited. Preliminary Report.

SNC-Lavalin (2014) Conceptual Engineering for Howse Water Management Plan. Technical Note. 622834-4000-40ER-0005. November 2014.

#### Notice to Reader

This report has been prepared and the work referred to in this report have been undertaken by SNC-Lavalin Inc., Environment & Geoscience (SNC-Lavalin GEM) for the exclusive use of Groupe Hémisphères (the Client), who has been party to the development of the scope of work and understands its limitations. The methodology, findings, conclusions and recommendations in this report are based solely upon the scope of work and subject to the time and budgetary considerations described in the proposal and/or contract pursuant to which this report was issued. Any use, reliance on, or decision made by a third party based on this report is the sole responsibility of such third party. SNC-Lavalin GEM accepts no liability or responsibility for any damages that may be suffered or incurred by any third party as a result of the use of, reliance on, or any decision made based on this report.

The findings, conclusions and recommendations in this report (i) have been developed in a manner consistent with the level of skill normally exercised by professionals currently practicing under similar conditions in the area, and (ii) reflect SNC-Lavalin GEM's best judgment based on information available at the time of preparation of this report. No other warranties, either expressed or implied, are made as to the professional services provided under the terms of our original contract and included in this report. The findings and conclusions contained in this report are valid only as of the date of this report and may be based, in part, upon information provided by others. If any of the information is inaccurate, new information is discovered, site conditions change or applicable standards are amended, modifications to this report may be necessary. The results of this assessment should in no way be construed as a warranty that the subject site is free from any and all contamination.

Any soil and rock descriptions in this report and associated logs have been made with the intent of providing general information on the subsurface conditions of the site. This information should not be used as geotechnical data for any purpose unless specifically addressed in the text of this report. Groundwater conditions described in this report refer only to those observed at the location and time of observation noted in the report.

This report must be read as a whole, as sections taken out of context may be misleading. If discrepancies occur between the preliminary (draft) and final version of this report, it is the final version that takes precedence. Nothing in this report is intended to constitute or provide a legal opinion.

The contents of this report are confidential and proprietary. Other than by the Client, copying or distribution of this report or use of or reliance on the information contained herein, in whole or in part, is not permitted without the express written permission of the Client and SNC-Lavalin GEM.

### Appendix A

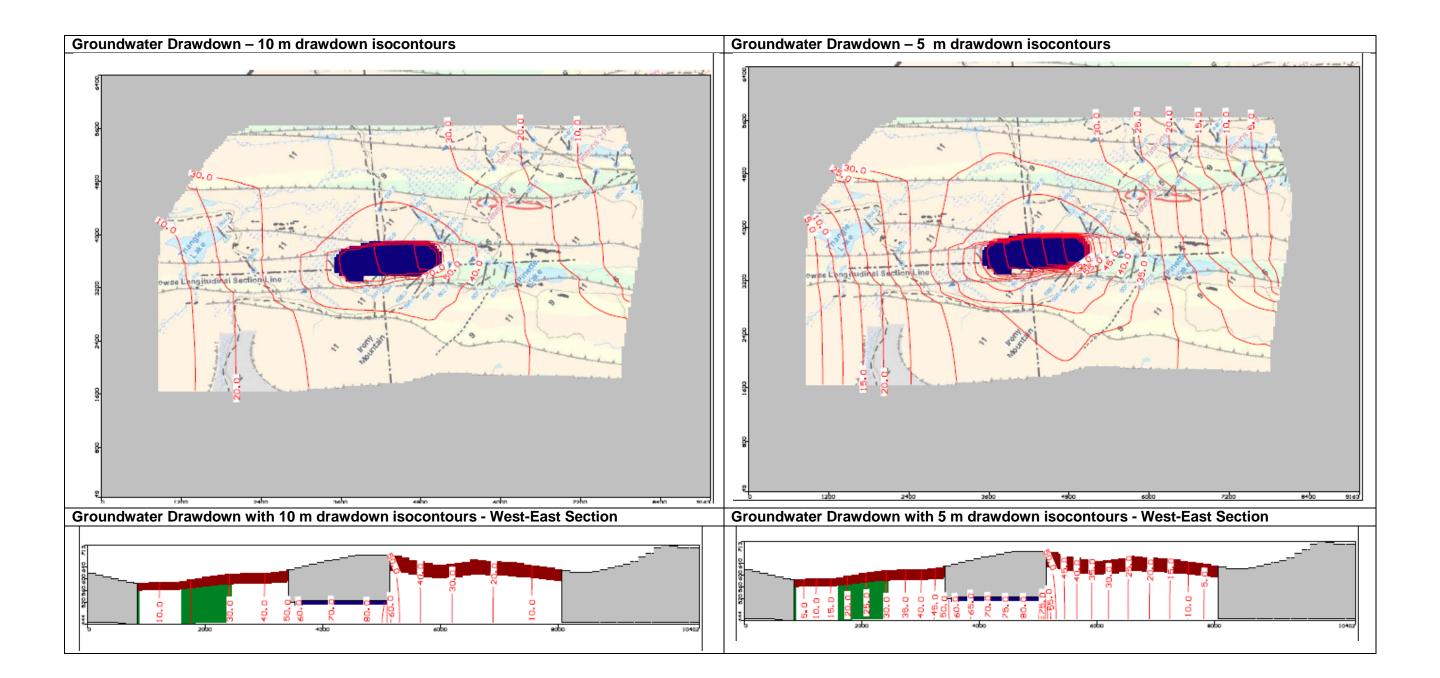
Modeling Results

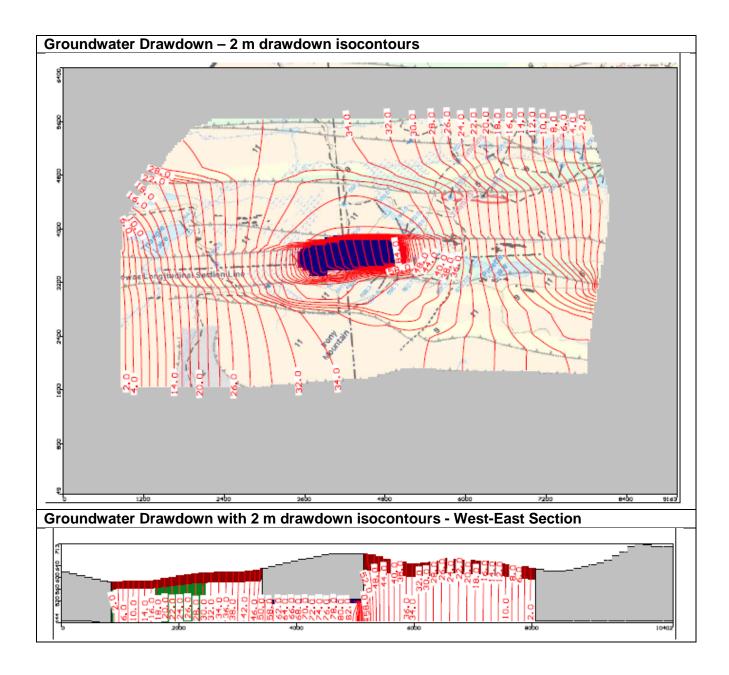
### Case 1 Kxyz of initial calibration + Recharged reduced to 60 mm/yr

	Kx (m/s)		Ky (m/s)		Kz (m/s)	
Zone	Calibrated	Sensitivity analysis	Calibrated	Sensitivity analysis	Calibrated	Sensitivity analysis
Overburden	1,00E-05	1,00E-05	1,00E-05	1,00E-05	1,00E-05	1,00E-05
Sokoman	9,40E-06	9,40E-06	9,40E-06	9,40E-06	9,40E-06	9,40E-06
Wishart	8,00E-07	8,00E-07	8,00E-07	8,00E-07	8,00E-07	8,00E-07
Shale	1,00E-07	1,00E-07	1,00E-07	1,00E-07	1,00E-07	1,00E-07
Faults zones	2,60E-07	2,60E-07	2,60E-07	2,60E-07	2,60E-07	2,60E-07

Table Sensitivity analysis – Case 1

Recharge (mm/year)	Calibrated	Sensitivity analysis
R(1)	100	60



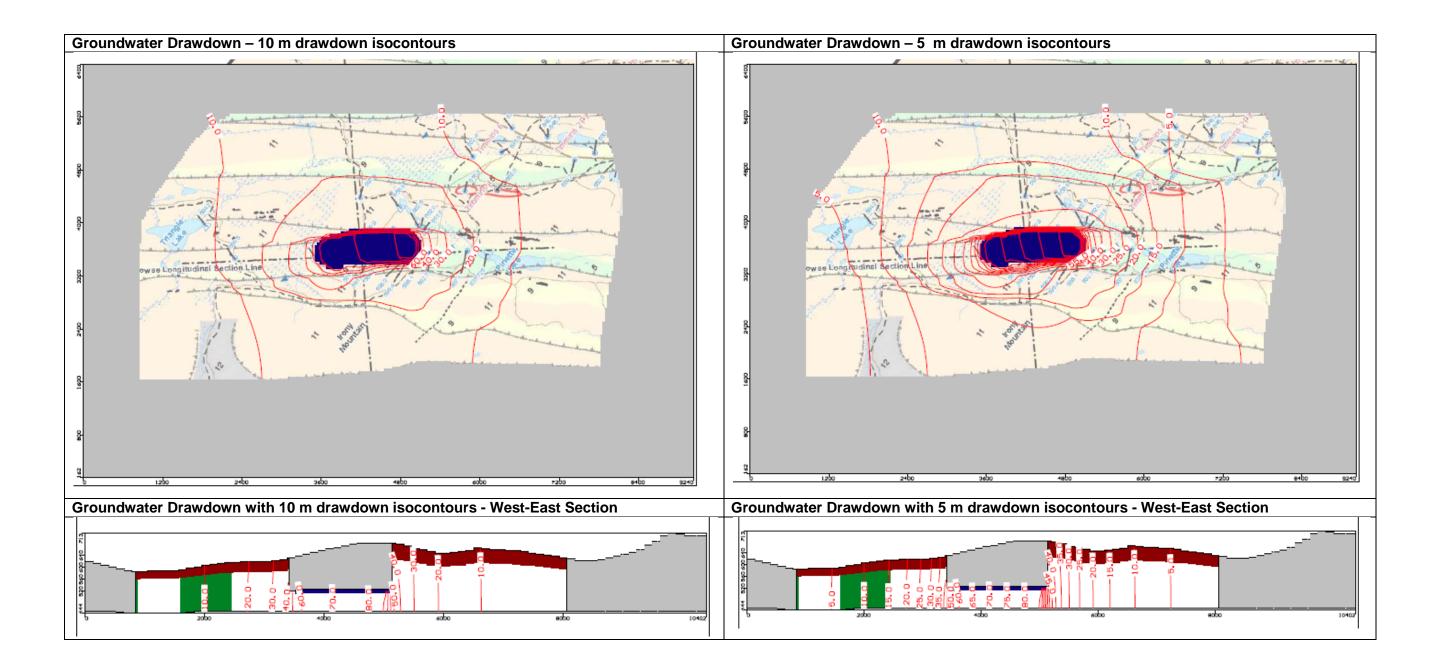


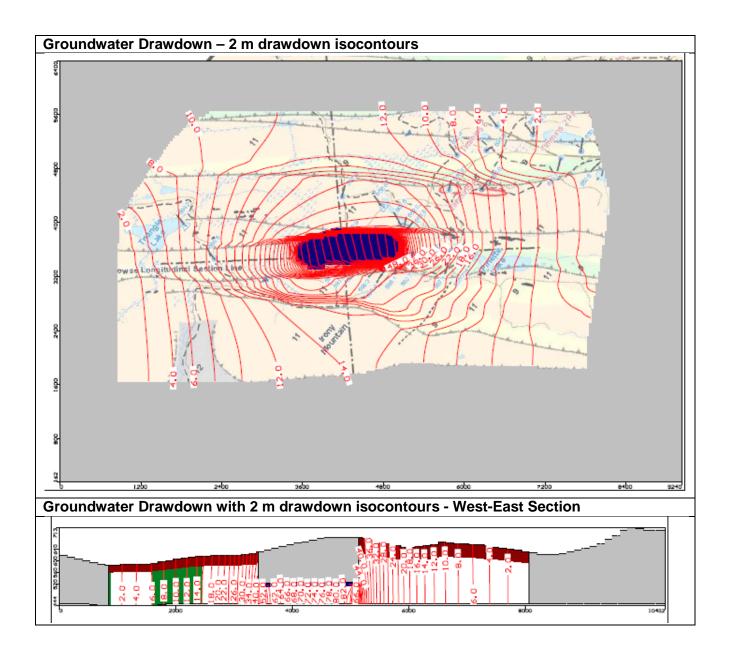
# Case 3 Kxyz of initial calibration + Recharged increased to 250 mm/yr

Table Se	nsitivity a	analysis	- Case 3
----------	-------------	----------	----------

	Kx (m/s)		Ky (m/s)		Kz (m/s)	
Zone	Calibrated	Sensitivity analysis	Calibrated	Sensitivity analysis	Calibrated	Sensitivity analysis
Overburden	1,00E-05	1,00E-05	1,00E-05	1,00E-05	1,00E-05	1,00E-05
Sokoman	9,40E-06	9,40E-06	9,40E-06	9,40E-06	9,40E-06	9,40E-06
Wishart	8,00E-07	8,00E-07	8,00E-07	8,00E-07	8,00E-07	8,00E-07
Shale	1,00E-07	1,00E-07	1,00E-07	1,00E-07	1,00E-07	1,00E-07
Faults zones	2,60E-07	2,60E-07	2,60E-07	2,60E-07	2,60E-07	2,60E-07

Recharge (mm/year)	Calibrated	Sensitivity analysis	
R(1)	100	250	



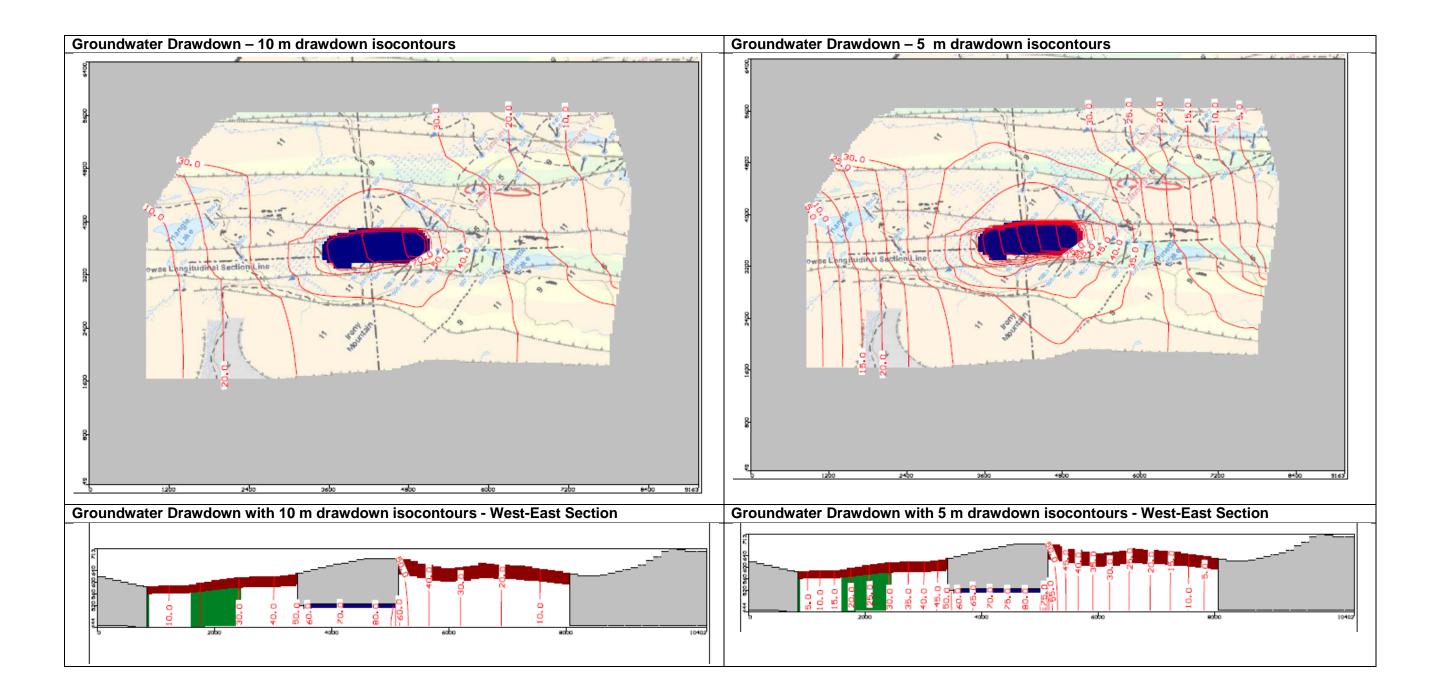


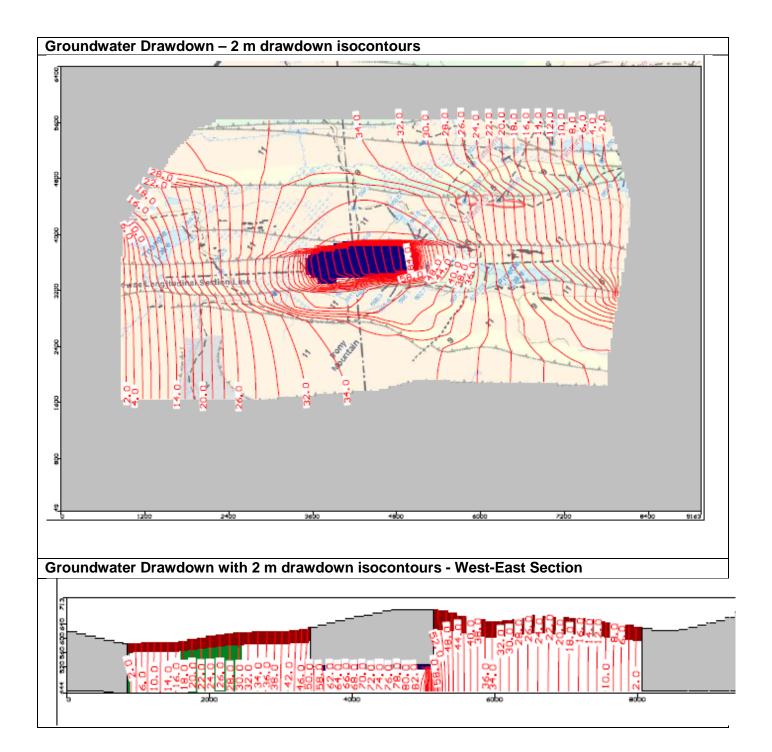
# Case 4: Increase Kxyz for the Sokoman and Overburden (x2) + Recharged decreased to 60 mm/yr

Table Sensitivity	analysis -	Case 4
-------------------	------------	--------

	Kx (m/s)		Ky (m/s)		Kz (m/s)	
Zone	Calibrated	Sensitivity analysis	Calibrated	Sensitivity analysis	Calibrated	Sensitivity analysis
Overburden	1,00E-05	2,00E-05	1,00E-05	2,00E-05	1,00E-05	2,00E-05
Sokoman	9,40E-06	1,88E-05	9,40E-06	1,88E-05	9,40E-06	1,88E-05
Wishart	8,00E-07	8,00E-07	8,00E-07	8,00E-07	8,00E-07	8,00E-07
Shale	1,00E-07	1,00E-07	1,00E-07	1,00E-07	1,00E-07	1,00E-07
Faults zones	2,60E-07	2,60E-07	2,60E-07	2,60E-07	2,60E-07	2,60E-07

Recharge (mm/year)	Calibrated	Sensitivity analysis	
R(1)	100	60	





# Case 6: Increase Kxyz for the Sokoman and Overburden (x2) + Recharged increased to 250 mm/yr

Zone	Kx (m/s)		Ky (m/s)		Kz (m/s)	
	Calibrated	Sensitivity analysis	Calibrated	Sensitivity analysis	Calibrated	Sensitivity analysis
Overburden	1,00E-05	2,00E-05	1,00E-05	2,00E-05	1,00E-05	2,00E-05
Sokoman	9,40E-06	1,88E-05	9,40E-06	1,88E-05	9,40E-06	1,88E-05
Wishart	8,00E-07	8,00E-07	8,00E-07	8,00E-07	8,00E-07	8,00E-07
Shale	1,00E-07	1,00E-07	1,00E-07	1,00E-07	1,00E-07	1,00E-07
Faults zones	2,60E-07	2,60E-07	2,60E-07	2,60E-07	2,60E-07	2,60E-07

Recharge (mm/year)	Calibrated	Sensitivity analysis	
R(1)	100	250	

